

# Low Cost, High Speed Rail-to-Rail Amplifiers

## AD8051/AD8052/AD8054

#### **FEATURES**

Low Cost Single (AD8051), Dual (AD8052), and Quad (AD8054) **Voltage Feedback Architecture** Fully Specified at +3 V, +5 V, and ±5 V Supplies Single-Supply Operation Output Swings to within 25 mV of Either Rail Input Voltage Range: -0.2 V to +4 V; V<sub>s</sub> = +5 V High Speed and Fast Settling on 5 V: 110 MHz -3 dB Bandwidth (G = +1) (AD8051/AD8052) 150 MHz -3 dB Bandwidth (G = +1) (AD8054) 145 V/µs Slew Rate 50 ns Settling Time to 0.1% **Small Packaging** AD8051 Available in SOT-23-5 AD8052 Available in MSOP-8 AD8054 Available in TSSOP-14 Good Video Specifications (G = +2) Gain Flatness of 0.1 dB to 20 MHz;  $R_1 = 150 \Omega$ 0.03% Differential Gain Error;  $R_L = 1 \ k\Omega$ 0.03° Differential Phase Error;  $R_L$  = 1 k $\Omega$ Low Distortion –80 dBc Total Harmonic @ 1 MHz,  $R_L$  = 100  $\Omega$ **Outstanding Load Drive Capability** Drives 45 mA, 0.5 V from Supply Rails (AD8051/AD8052) Drives 50 pF Capacitive Load (G = +1) (AD8051/AD8052) Low Power of 2.75 mA/Amplifier (AD8054) Low Power of 4.4 mA/Amplifier (AD8051/AD8052)

APPLICATIONS Coax Cable Drivers Active Filters Video Switchers A/D Driver Professional Cameras CCD Imaging Systems CD/DVD ROMs

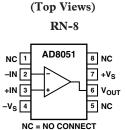
#### **GENERAL DESCRIPTION**

The AD8051 (single), AD8052 (dual), and AD8054 (quad) are low cost, voltage feedback, high speed amplifiers designed to operate on +3 V, +5 V, or  $\pm$ 5 V supplies. They have true singlesupply capability with an input voltage range extending 200 mV below the negative rail and within 1 V of the positive rail.

Despite their low cost, the AD8051/AD8052/AD8054 provide excellent overall performance and versatility. The output voltage swing extends to within 25 mV of each rail, providing the maximum output dynamic range with excellent overdrive recovery.

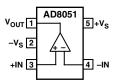
#### REV. D

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**PIN CONNECTIONS** 

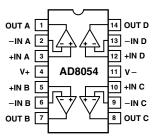




RN-8, MSOP (RM)

OUT1 1	AD80	52	8 +V <sub>S</sub>
-IN1 2	4		7 OUT
+IN1 3			6 –IN2
-V <sub>S</sub> 4	$\leq$	╤┷	5 +IN2

#### RN-14, TSSOP-14 (RU-14)



This makes the AD8051/AD8052/AD8054 useful for video electronics, such as cameras, video switchers, or any high speed portable equipment. Low distortion and fast settling make them ideal for active filter applications.

The AD8051/AD8052/AD8054 offer low power supply current and can operate on a single 3 V power supply. These features are ideally suited for portable and battery-powered applications where size and power are critical.

The wide bandwidth and fast slew rate on a single +5 V supply make these amplifiers useful in many general-purpose, high speed applications where dual power supplies of up to  $\pm 6$  V and single supplies from +3 V to +12 V are needed.

All of this low cost performance is offered in an 8-lead SOIC, as well as a tiny SOT-23-5 package (AD8051), an MSOP package (AD8052), and a TSSOP-14 (AD8054). The AD8051 and AD8052 in the SOIC-8 and RM packages are available in the extended temperature range of  $-40^{\circ}$ C to  $+125^{\circ}$ C.

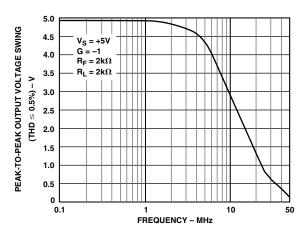


Figure 1. Low Distortion Rail-to-Rail Output Swing

# **SPECIFICATIONS** (@ $T_A = 25^{\circ}$ C, $V_S = 5$ V, $R_L = 2$ k $\Omega$ to 2.5 V, unless otherwise noted.)

		AD8051A/AD8052A			AD8054A			1
Parameter	Conditions	Min	Тур	Max	Min	Тур	Max	Unit
DYNAMIC PERFORMANCE								
	$G = \pm 1$ $W = 0.2$ $W = 0$	70	110		80	150		MHz
-3 dB Small Signal Bandwidth	$G = +1, V_0 = 0.2 V p-p$	10			80			
	$G = -1, +2, V_0 = 0.2 V p-p$		50			60		MHz
Bandwidth for 0.1 dB Flatness	$G = +2, V_0 = 0.2 V p-p,$							
	$R_{\rm L} = 150 \ \Omega$ to 2.5 V,							
	$R_F = 806 \Omega$ for AD8051A/							
	AD8052A		20					MHz
	$R_{\rm F} = 200 \ \Omega$ for AD8054A					12		MHz
Slew Rate	$G = -1$ , $V_0 = 2$ V Step	100	145		140	170		V/µs
Full Power Response	$G = +1, V_0 = 2 V p - p$	100	35		140	45		MHz
Settling Time to 0.1%	$G = -1, V_0 = 2 V Step$		50			40		ns
NOISE/DISTORTION PERFORMANCE								
Total Harmonic Distortion*	$f_{C} = 5 \text{ MHz}, V_{O} = 2 \text{ V p-p}, G = +2$		-67			-68		dB
Input Voltage Noise	f = 10  kHz		16			16		nV/√Hz
Input Current Noise	f = 10  kHz		850			850		$fA/\sqrt{Hz}$
-								
Differential Gain Error (NTSC)	$G = +2, R_L = 150 \Omega$ to 2.5 V		0.09			0.07		%
	$R_L = 1 \ k\Omega$ to 2.5 V		0.03			0.02		%
Differential Phase Error (NTSC)	$G = +2, R_L = 150 \Omega$ to 2.5 V		0.19			0.26		Degrees
	$R_L = 1 \ k\Omega$ to 2.5 V		0.03			0.05		Degrees
Crosstalk	f = 5 MHz, G = +2		-60			-60		dB
DC PERFORMANCE			17	10		17	10	
Input Offset Voltage			1.7	10		1.7	12	mV
	T <sub>MIN</sub> -T <sub>MAX</sub>			25			30	mV
Offset Drift			10			15		µV/°C
Input Bias Current			1.4	2.5		2	4.5	μA
	T <sub>MIN</sub> -T <sub>MAX</sub>			3.25			4.5	μA
Input Offset Current			0.1	0.75		0.2	1.2	μA
Open-Loop Gain	$R_{\rm L} = 2 \ k\Omega$ to 2.5 V	86	98		82	98		dB
I I I I I I I I I I I I I I I I I I I	T <sub>MIN</sub> -T <sub>MAX</sub>		96			96		dB
	$R_{\rm L} = 150 \Omega$ to 2.5 V	76	82		74	82		dB
	$T_{MIN} - T_{MAX}$	10	78		11	78		dB
	MIN MAA		-			-		
INPUT CHARACTERISTICS								
Input Resistance			290			300		kΩ
Input Capacitance			1.4			1.5		pF
Input Common-Mode Voltage Range			-0.2 to +4			-0.2 to +4		V
Common-Mode Rejection Ratio	$V_{CM} = 0 V \text{ to } 3.5 V$	72	88		70	86		dB
OUTPUT CHARACTERISTICS	$\mathbf{P} = 10 \pm 0 \pm 0.5 \text{ V}$		0.015 . 4.005			0.02 + 4.077		N.
Output Voltage Swing	$R_L = 10 \text{ k}\Omega \text{ to } 2.5 \text{ V}$		0.015 to 4.985			0.03 to 4.975		V
	$R_L = 2 k\Omega$ to 2.5 V	0.1 to 4.9	0.025 to 4.975		0.125 to 4.875	0.05 to 4.95		V
	$R_L = 150 \Omega$ to 2.5 V	0.3 to 4.625	0.2 to 4.8		0.55 to 4.4	0.25 to 4.65		V
Output Current	$V_{OUT} = 0.5 V \text{ to } 4.5 V$		45			30		mA
•	T <sub>MIN</sub> -T <sub>MAX</sub>		45			30		mA
Short-Circuit Current	Sourcing		80			45		mA
	Sinking		130			85		mA
Capacitive Load Drive	G = +1 (AD8051/AD8052)		50			00		pF
Capacitive Load Drive	G = +2 (AD8054)		50			40		pF
						-		r
POWER SUPPLY								
Operating Range		3		12	3		12	V
Quiescent Current/Amplifier			4.4	5		2.75	3.275	mA
Power Supply Rejection Ratio	$\Delta V_{S} = \pm 1 V$	70	80		68	80		dB
OPERATING TEMPERATURE RANGE	RT, RU,							
OF ENATING TEMPERATURE RANGE	RN-14	-40		+85	-40		+85	°C
	RM, RN-8	-40		+125	UF U		101	°C
		1 -40		+125	1			. <b>≃</b> .

\*Refer to TPC 13.

Specifications subject to change without notice.

# AD8051/AD8052/AD8054 **SPECIFICATIONS** (@ $T_A = 25^{\circ}C$ , $V_S = 3 V$ , $R_L = 2 k\Omega$ to 1.5 V, unless otherwise noted.)

		AD8051A/AD8052A			AD8054A			
Parameter	Conditions	Min	Тур	Max	Min	Тур	Max	Unit
DYNAMIC PERFORMANCE								
-3 dB Small Signal Bandwidth	$G = +1, V_0 = 0.2 V p-p$	70	110		80	135		MHz
	$G = -1, +2, V_0 = 0.2 V p-p$		50			65		MHz
Bandwidth for 0.1 dB Flatness	$G = +2, V_0 = 0.2 V p-p,$		50			05		
	$R_{\rm L} = 150 \ \Omega \ \text{to} \ 2.5 \ \text{V},$							
	$R_{\rm F} = 402 \ \Omega$ for AD8051A/AD8052A		17					MHz
	$R_F = 200 \Omega$ for AD8054A		17			10		MHz
Slew Rate	$G = -1, V_0 = 2 V Step$	90	135		110	150		V/µs
Full Power Response	$G = +1, V_0 = 1 V p-p$	50	65		110	85		MHz
Settling Time to 0.1%	$G = -1, V_0 = 2 V Step$		55			55		ns
			55					115
NOISE/DISTORTION PERFORMANCE								
Total Harmonic Distortion*	$f_{\rm C} = 5$ MHz, $V_{\rm O} = 2$ V p-p,							
	$G = -1, R_L = 100 \Omega$ to 1.5 V		-47			-48		dB
Input Voltage Noise	f = 10  kHz		16			16		nV/√Hz
Input Current Noise	f = 10  kHz		600			600		fA/√Hz
Differential Gain Error (NTSC)	$G = +2, V_{CM} = 1 V$							
	$R_{\rm L} = 150 \ \Omega$ to 1.5 V,		0.11			0.13		%
	$R_L = 1 \ k\Omega$ to 1.5 V		0.09			0.09		%
Differential Phase Error (NTSC)	$G = +2, V_{CM} = 1 V$							
	$R_L = 150 \Omega$ to 1.5 V		0.24			0.3		Degrees
	$R_L = 1 k\Omega$ to 1.5 V		0.10			0.1		Degrees
Crosstalk	f = 5 MHz, G = +2		-60			-60		dB
DC PERFORMANCE								
Input Offset Voltage			1.6	10		1.6	12	mV
	T <sub>MIN</sub> -T <sub>MAX</sub>			25			30	mV
Offset Drift			10			15		μV/°C
Input Bias Current			1.3	2.6		2	4.5	μA
	T <sub>MIN</sub> -T <sub>MAX</sub>			3.25			4.5	μA
Input Offset Current			0.15	0.8		0.2	1.2	μA
Open-Loop Gain	$R_L = 2 k\Omega$	80	96		80	96		dB
	T <sub>MIN</sub> -T <sub>MAX</sub>		94			94		dB
	$R_L = 150 \Omega$	74	82		72	80		dB
	$T_{MIN}-T_{MAX}$		76			76		dB
INPUT CHARACTERISTICS								
Input Resistance			290			300		kΩ
Input Capacitance			1.4			1.5		pF
Input Common-Mode Voltage Range			-0.2 to +2			-0.2 to +2		v
Common-Mode Rejection Ratio	$V_{CM} = 0 V$ to 1.5 V	72	88		70	86		dB
OUTPUT CHARACTERISTICS								
Output Voltage Swing	$R_{\rm L} = 10 \ \rm k\Omega$ to 1.5 V		0.01 to 2.99			0.025 to 2.98		v
fat i onage omnig	$R_{\rm L} = 2 \ k\Omega \ \text{to} \ 1.5 \ \text{V}$	0.075 to 2.9	0.02 to 2.98		0.1 to 2.9	0.35 to 2.965		v
	$R_L = 150 \Omega$ to 1.5 V	0.2 to 2.75	0.125 to 2.875		0.35 to 2.55	0.15 to 2.75		v
Output Current	$V_{OUT} = 0.5 \text{ V to } 2.5 \text{ V}$	5.2 (5 2.15	45			25		mA
pat Guitent	$T_{MIN}-T_{MAX}$		45			25		mA
Short-Circuit Current	Sourcing		60			30		mA
choir oneur ourent	Sinking		90			50		mA
Capacitive Load Drive	G = +1 (AD8051/AD8052)		45					pF
Supusitive Louis Drive	G = +2 (AD8054)		13			35		pF
POWER SUPPLY								
Operating Range		3		12	3		12	v
Quiescent Current/Amplifier		ر	4.2	12 4.8	ر	2.625	12 3.125	v mA
Power Supply Rejection Ratio	$\Delta V_{S} = 0.5 V$	68	4.2 80	ч.0	68	80	5.125	dB
								u D
OPERATING TEMPERATURE RANGE	RT, RU,	40		105	40		105	
	RN-14	-40		+85	-40		+85	°C
	RM, RN-8	-40		+125	1			°C

\*Refer to TPC 13.

Specifications subject to change without notice.

# $\label{eq:spectrum} SPECIFICATIONS \quad (@\ T_A = 25^\circ C,\ V_S = \pm 5\ V,\ R_L = 2\ k\Omega \ to \ Ground,\ unless \ otherwise \ noted.)$

		AD8051A/AD8052A			AD8054A			
Parameter	Conditions	Min	Тур	Max	Min	Тур	Max	Unit
DYNAMIC PERFORMANCE	C = 11 $W = 0.2$ $W = 0.2$	70	110		95	160		MIL
-3 dB Small Signal Bandwidth	$G = +1, V_0 = 0.2 V p-p$	70	110		85	160		MHz
	$G = -1, +2, V_O = 0.2 V p-p$		50			65		MHz
Bandwidth for 0.1 dB Flatness	$G = +2, V_0 = 0.2 V p-p,$							
	$R_L = 150 \Omega$ ,							
	$R_{\rm F} = 1.1 \ \rm k\Omega$ for							
	AD8051A/AD8052A		20					MHz
	$R_{\rm F} = 200 \ \Omega$ for AD8054A					15		MHz
Slew Rate	$G = -1$ , $V_O = 2$ V Step	105	170		150	190		V/µs
Full Power Response	$G = +1, V_0 = 2 V p-p$		40			50		MHz
Settling Time to 0.1%	$G = -1$ , $V_O = 2$ V Step		50			40		ns
NOISE/DISTORTION PERFORMANCE								
Total Harmonic Distortion	$f_{C} = 5$ MHz, $V_{O} = 2$ V p-p, $G = +2$		-71			-72		dB
Input Voltage Noise	f = 10  kHz		16			16		nV/\(\nV
Input Current Noise	f = 10  kHz		900			900		fA/√Hz
Differential Gain Error (NTSC)	$G = +2, R_L = 150 \Omega$		0.02			0.06		%
	$R_{\rm L} = 1 \ k\Omega$		0.02			0.02		%
Differential Phase Error (NTSC)	$G = +2, R_{\rm L} = 150 \ \Omega$		0.11			0.15		Degrees
Differential Thase Error (1415C)	$R_{\rm I} = 1 \ k\Omega$		0.02			0.03		Degrees
Crosstalk	f = 5  MHz, G = +2		-60			-60		dB
	1 - 5 Milz, G - 12		00			00		
DC PERFORMANCE								
Input Offset Voltage			1.8	11		1.8	13	mV
	T <sub>MIN</sub> -T <sub>MAX</sub>			27			32	mV
Offset Drift			10			15		µV/°C
Input Bias Current			1.4	2.6		2	4.5	μA
	T <sub>MIN</sub> -T <sub>MAX</sub>			3.5			4.5	μA
Input Offset Current			0.1	0.75		0.2	1.2	μA
Open-Loop Gain	$R_L = 2 k\Omega$	88	96		84	96		dB
	T <sub>MIN</sub> -T <sub>MAX</sub>		96			96		dB
	$R_L = 150 \Omega$	78	82		76	82		dB
	T <sub>MIN</sub> -T <sub>MAX</sub>		80			80		dB
INPUT CHARACTERISTICS								
Input Resistance			290			300		kΩ
Input Capacitance			1.4			1.5		pF
								V
Input Common-Mode Voltage Range	V = 5 V + 12 5 V	70	-5.2 to +4		70	-5.2 to +4		
Common-Mode Rejection Ratio	$V_{CM} = -5 V \text{ to } +3.5 V$	72	88		70	86		dB
OUTPUT CHARACTERISTICS								
Output Voltage Swing	$R_L = 10 \ k\Omega$		-4.98 to +4.98			-4.97 to +4.97		V
	$R_L = 2 k\Omega$	-4.85 to +4.85	-4.97 to +4.97		-4.8 to +4.8	-4.9 to +4.9		v
	$R_L = 150 \Omega$	-4.45 to +4.3	-4.6 to +4.6		-4.0 to +3.8	-4.5 to +4.5		V
Output Current	$V_{OUT} = -4.5 \text{ V}$ to +4.5 V		45			30		mA
	T <sub>MIN</sub> -T <sub>MAX</sub>		45			30		mA
Short-Circuit Current	Sourcing		100			60		mA
	Sinking		160			100		mA
Capacitive Load Drive	G = +1 (AD8051/AD8052)		50					pF
	G = +2 (AD8054)					40		pF
DOWED SUDDI V								
POWER SUPPLY		2		10	2		10	
Operating Range		3	1.0	12	3		12	V.
Quiescent Current/Amplifier			4.8	5.5		2.875	3.4	mA
Power Supply Rejection Ratio	$\Delta V_{S} = \pm 1 V$	68	80		68	80		dB
OPERATING TEMPERATURE RANGE	RT, RU,							
					1			1
	RN-14	-40		+85	-40		+85	°C

Specifications subject to change without notice.

#### ABSOLUTE MAXIMUM RATINGS<sup>1</sup>

Supply Voltage 12.6 V
Internal Power Dissipation <sup>2</sup>
Small Outline Package (RN) Observe Power Derating Curves
SOT-23-5 Package Observe Power Derating Curves
MSOP Package Observe Power Derating Curves
TSSOP-14 Package Observe Power Derating Curves
Input Voltage (Common Mode) $\dots \dots \dots \pm V_S$
Differential Input Voltage ±2.5 V
Output Short Circuit Duration

..... Observe Power Derating Curves Storage Temperature Range (RN) ..... -65°C to +150°C Operating Temperature Range (A Grade) ... -40°C to +125°C Lead Temperature Range (Soldering 10 sec) ..... 300°C NOTES

<sup>1</sup> Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. This is a stress rating only; functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

<sup>2</sup> Specification is for device in free air:  $P_{1} = 125$ °C/W

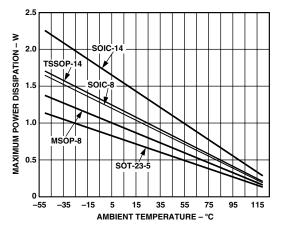
8-Lead SOIC:  $\theta_{JA} = 125^{\circ}C/W$ 5-Lead SOT-23-5:  $\theta_{JA} = 180^{\circ}C/W$ 8-Lead MSOP:  $\theta_{JA} = 150^{\circ}C/W$ 14-Lead SOIC:  $\theta_{JA} = 90^{\circ}C/W$ 14-Lead TSSOP:  $\theta_{JA} = 120^{\circ}C/W$ 

#### MAXIMUM POWER DISSIPATION

The maximum power that can be safely dissipated by the AD8051/AD8052/AD8054 is limited by the associated rise in junction temperature. The maximum safe junction temperature

for plastic encapsulated devices is determined by the glass transition temperature of the plastic, approximately 150°C. Temporarily exceeding this limit may cause a shift in parametric performance due to a change in the stresses exerted on the die by the package. Exceeding a junction temperature of 175°C for an extended period can result in device failure.

While the AD8051/AD8052/AD8054 are internally short-circuit protected, this may not be sufficient to guarantee that the maximum junction temperature (150°C) is not exceeded under all conditions. To ensure proper operation, it is necessary to observe the maximum power derating curves.



*Figure 2. Plot of Maximum Power Dissipation vs. Temperature for AD8051/AD8052/AD8054* 

Model Temperature Range		Package Descriptions	Package Options*	Brand Code			
AD8051AR AD8051AR-REEL AD8051AR-REEL7 AD8051ART-REEL AD8051ART-REEL7	-40°C to +125°C -40°C to +125°C -40°C to +125°C -40°C to +125°C -40°C to +85°C -40°C to +85°C	8-Lead SOIC 13" Tape and Reel 7" Tape and Reel 13" Tape and Reel 7" Tape and Reel	RN-8 RN-8 RN-8 RT-5 RT-5	H2A H2A			
AD8052AR AD8052AR-REEL AD8052AR-REEL7 AD8052ARM AD8052ARM-REEL AD8052ARM-REEL7	-40°C to +125°C -40°C to +125°C -40°C to +125°C -40°C to +125°C -40°C to +125°C -40°C to +125°C -40°C to +125°C	8-Lead SOIC 13" Tape and Reel 7" Tape and Reel 8-Lead MSOP 13" Tape and Reel 7" Tape and Reel	RN-8 RN-8 RN-8 RM-8 RM-8 RM-8	H4A H4A H4A			
AD8054AR AD8054AR-REEL AD8054AR-REEL7 AD8054ARU AD8054ARU-REEL AD8054ARU-REEL7	-40°C to +85°C -40°C to +85°C -40°C to +85°C -40°C to +85°C -40°C to +85°C -40°C to +85°C -40°C to +85°C	14-Lead SOIC 13" Tape and Reel 7" Tape and Reel 14-Lead MSOP 13" Tape and Reel 7" Tape and Reel	RN-14 RN-14 RN-14 RU-14 RU-14 RU-14				

**ORDERING GUIDE** 

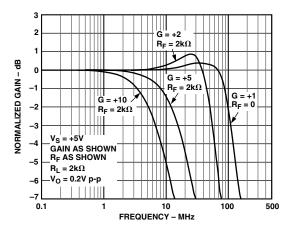
\*RN = Small Outline; RM = MSOP; RT = Surface Mount; RU = TSSOP.

#### CAUTION \_

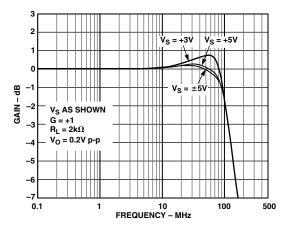
ESD (electrostatic discharge) sensitive device. Electrostatic charges as high as 4000 V readily accumulate on the human body and test equipment and can discharge without detection. Although the AD8051/AD8052/AD8054 feature proprietary ESD protection circuitry, permanent damage may occur on devices subjected to high energy electrostatic discharges. Therefore, proper ESD precautions are recommended to avoid performance degradation or loss of functionality.



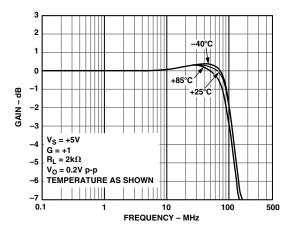
### Typical Performance Characteristics-AD8051/AD8052/AD8054



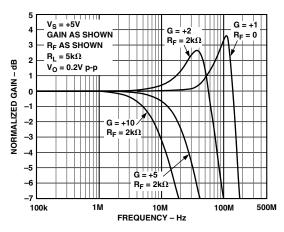
TPC 1. AD8051/AD8052 Normalized Gain vs. Frequency;  $V_S = +5 V$ 



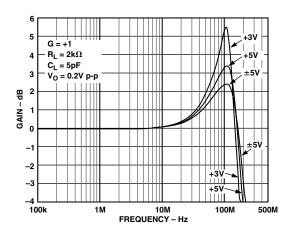
TPC 2. AD8051/AD8052 Gain vs. Frequency vs. Supply



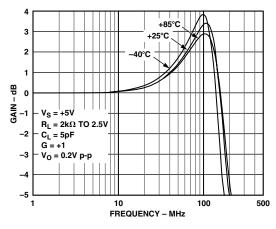
TPC 3. AD8051/AD8052 Gain vs. Frequency vs. Temperature



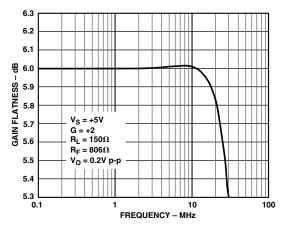
TPC 4. AD8054 Normalized Gain vs. Frequency;  $V_S = +5 V$ 



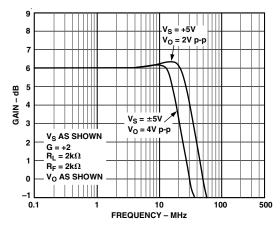
TPC 5. AD8054 Gain vs. Frequency vs. Supply



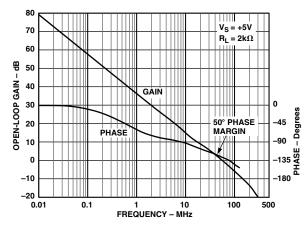
*TPC 6. AD8054 Gain vs. Frequency vs. Temperature* 



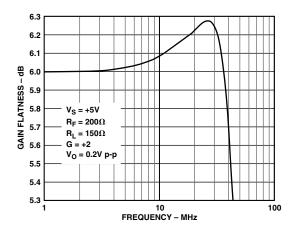
TPC 7. AD8051/AD8052 0.1 dB Gain Flatness vs. Frequency; G = +2



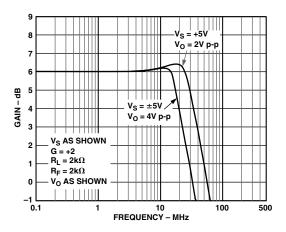
TPC 8. AD8051/AD8052 Large Signal Frequency Response; G = +2



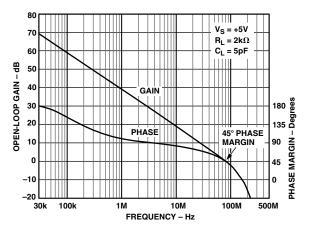
TPC 9. AD8051/AD8052 Open-Loop Gain and Phase vs. Frequency



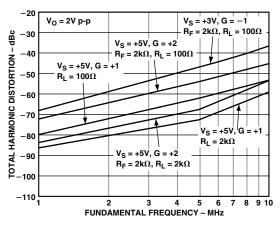
TPC 10. AD8054 0.1 dB Gain Flatness vs. Frequency; G = +2



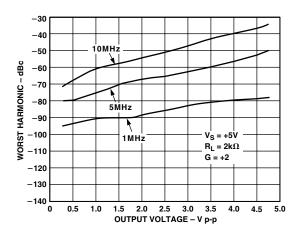
TPC 11. AD8054 Large Signal Frequency Response; G = +2



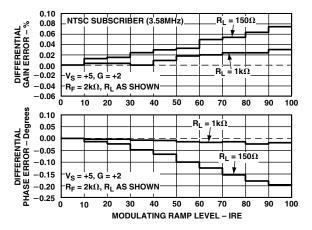
TPC 12. AD8054 Open-Loop Gain and Phase Margin vs. Frequency



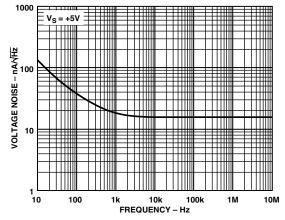
TPC 13. Total Harmonic Distortion



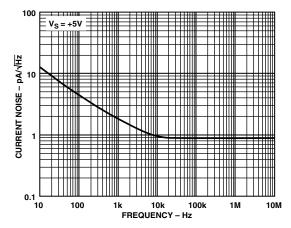
TPC 14. Worst Harmonic vs. Output Voltage



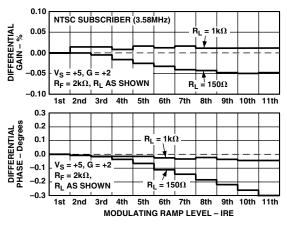
TPC 15. AD8051/AD8052 Differential Gain and Phase Errors



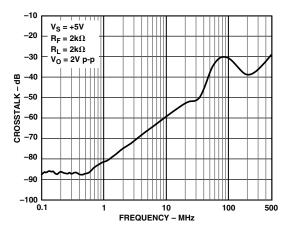
TPC 16. Input Voltage Noise vs. Frequency



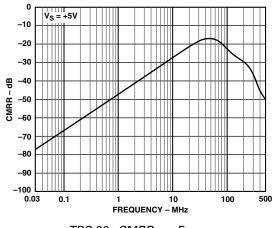
TPC 17. Input Current Noise vs. Frequency



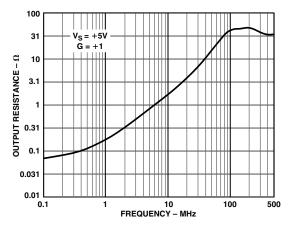
TPC 18. AD8054 Differential Gain and Phase Errors



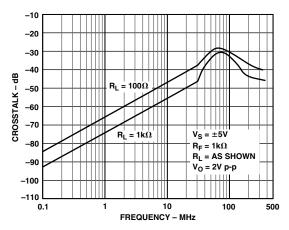
TPC 19. AD8052 Crosstalk (Output-to-Output) vs. Frequency



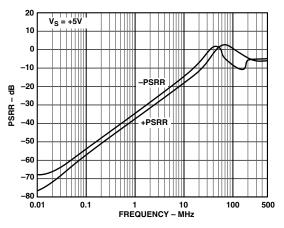
TPC 20. CMRR vs. Frequency



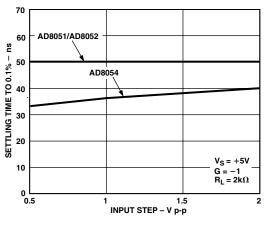
TPC 21. Closed-Loop Output Resistance vs. Frequency



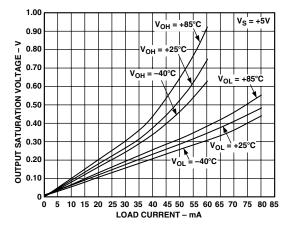
TPC 22. AD8054 Crosstalk (Output-to-Output) vs. Frequency



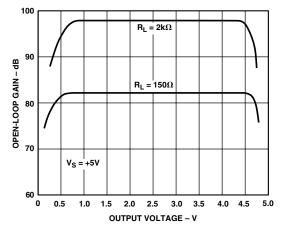
TPC 23. PSRR vs. Frequency



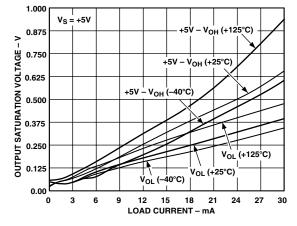
TPC 24. Settling Time vs. Input Step



TPC 25. AD8051/AD8052 Output Saturation Voltage vs. Load Current



TPC 26. Open-Loop Gain vs. Output Voltage



TPC 27. AD8054 Output Saturation Voltage vs. Load Current

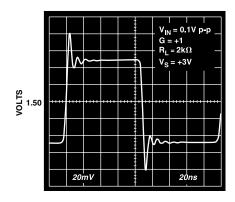


Figure 3. 100 mV Step Response, G = +1

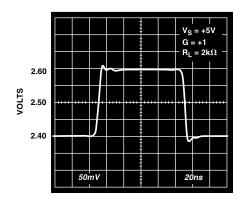


Figure 4. AD8051/AD8052 200 mV Step Response;  $V_S = +5 V$ , G = +1

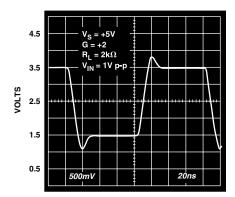


Figure 5. Large Signal Step Response;  $V_S = +5 V$ , G = +2

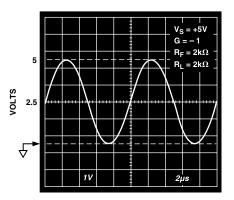


Figure 6. Output Swing; G = -1,  $R_L = +2 \ k\Omega$ 

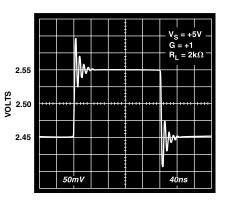


Figure 7. AD8054 100 mV Step Response;  $V_S = +5 V$ , G = +1

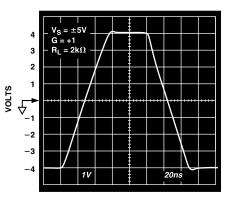


Figure 8. Large Signal Step Response;  $V_S = \pm 5 V, G = +1$ 

#### **Overdrive Recovery**

Overdrive of an amplifier occurs when the output and/or input range is exceeded. The amplifier must recover from this overdrive condition. As shown in Figure 9, the AD8051/AD8052/AD8054 recovers within 60 ns from negative overdrive and within 45 ns from positive overdrive.

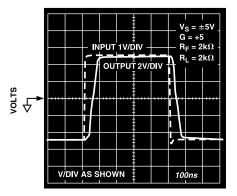


Figure 9. Overdrive Recovery

#### **Driving Capacitive Loads**

Consider the AD8051/AD8052 in a closed-loop gain of +1 with  $+V_s = 5$  V and a load of 2 k $\Omega$  in parallel with 50 pF. Figures 10 and 11 show its frequency and time domain responses, respectively, to a small-signal excitation. The capacitive load drive of the AD8051/AD8052/AD8054 can be increased by adding a low value resistor in series with the load. Figures 12 and 13 show the effect of a series resistor on the capacitive drive for varying voltage gains. As the closed-loop gain is increased, the larger phase margin allows for larger capacitive loads with less peaking. Adding a series resistor with lower closed-loop gains accomplishes the same effect. For large capacitive loads, the frequency response of the amplifier will be dominated by the roll-off of the series resistor and the load capacitance.

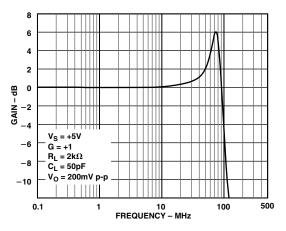


Figure 10. AD8051/AD8052 Closed-Loop Frequency Response:  $C_L = 50 \text{ pF}$ 

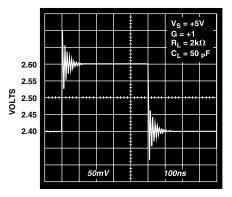


Figure 11. AD8051/AD8052 200 mV Step Response:  $C_L = 50 \text{ pF}$ 

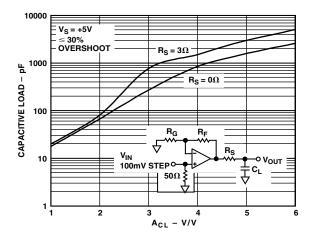


Figure 12. AD8051/AD8052 Capacitive Load Drive vs. Closed-Loop Gain

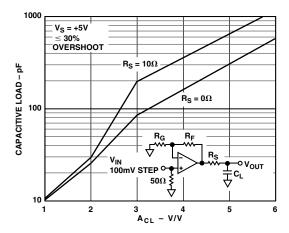


Figure 13. AD8054 Capacitive Load Drive vs. Closed-Loop Gain

#### **Circuit Description**

The AD8051/AD8052/AD8054 is fabricated on the Analog Devices proprietary eXtra-Fast Complementary Bipolar (XFCB) process, which enables the construction of PNP and NPN transistors with similar  $f_{\rm T}$ s in the 2 GHz to 4 GHz region. The process is dielectrically isolated to eliminate the parasitic and latch-up

problems caused by junction isolation. These features allow the construction of high frequency, low distortion amplifiers with low supply currents. This design uses a differential output input stage to maximize bandwidth and headroom (see Figure 14). The smaller signal swings required on the first stage outputs (nodes SIP, SIN) reduce the effect of nonlinear currents due to junction capacitances and improve the distortion performance. This design achieves harmonic distortion of  $-80 \ \text{dBc}$  @ 1 MHz into  $100 \ \Omega$  with  $V_{\text{OUT}} = 2 \ \text{V}$  p-p (Gain = +1) on a single 5 V supply.

The inputs of the device can handle voltages from -0.2 V below the negative rail to within 1 V of the positive rail. Exceeding these values will not cause phase reversal; however, the input ESD devices will begin to conduct if the input voltages exceed the rails by greater than 0.5 V. During this overdrive condition, the output stays at the rail.

The rail-to-rail output range of the AD8051/AD8052/AD8054 is provided by a complementary common-emitter output stage. High output drive capability is provided by injecting all output stage predriver currents directly into the bases of the output devices Q8 and Q36. Biasing of Q8 and Q36 is accomplished by I8 and I5, along with a common-mode feedback loop (not shown). This circuit topology allows the AD8051/AD8052 to drive 45 mA of output current and allows the AD8054 to drive 30 mA of output current with the outputs within 0.5 V of the supply rails.

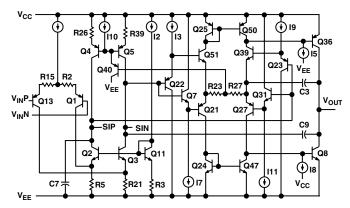


Figure 14. AD8051/AD8052 Simplified Schematic

#### APPLICATIONS

#### Layout Considerations

The specified high speed performance of the AD8051/AD8052/ AD8054 requires careful attention to board layout and component selection. Proper RF design techniques and low parasitic component selection are necessary.

The PCB should have a ground plane covering all unused portions of the component side of the board to provide a low impedance path. The ground plane should be removed from the area near the input pins to reduce parasitic capacitance.

Chip capacitors should be used for supply bypassing. One end should be connected to the ground plane and the other within 3 mm of each power pin. An additional large (4.7  $\mu$ F to 10  $\mu$ F) tantalum electrolytic capacitor should be connected in parallel, but not necessarily so close, to supply current for fast, large signal changes at the output.

The feedback resistor should be located close to the inverting input pin to keep the parasitic capacitance at this node to a

minimum. Parasitic capacitance of less than 1 pF at the inverting input can significantly affect high speed performance.

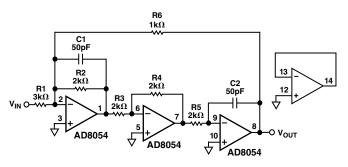
Stripline design techniques should be used for long signal traces (greater than about 25 mm). These should be designed with a characteristic impedance of 50  $\Omega$  or 75  $\Omega$  and be properly terminated at each end.

#### **Active Filters**

Active filters at higher frequencies require wider bandwidth op amps to work effectively. Excessive phase shift produced by lower frequency op amps can significantly impact active filter performance.

Figure 15 shows an example of a 2 MHz biquad bandwidth filter that uses three op amps of an AD8054. Such circuits are sometimes used in medical ultrasound systems to lower the noise bandwidth of the analog signal before A/D conversion.

Note that the unused amplifier's inputs should be tied to ground.



*Figure 15. 2 MHz Biquad Band-Pass Filter Using AD8054* The frequency response of the circuit is shown in Figure 16.

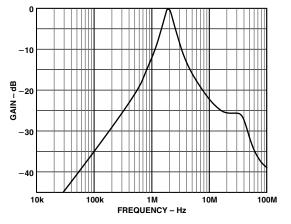


Figure 16. Frequency Response of 2 MHz Band-Pass Biquad Filter

#### A/D and D/A Applications

Figure 17 is a schematic showing the AD8051 used as a driver for an AD9201, a 10-bit 20 MSPS dual A/D converter. This converter is designed to convert I and Q signals in communication systems. In this application, only the I channel is being driven. The I channel is enabled by applying a logic HIGH to SELECT, Pin 13.

The AD8051 is running from a dual supply and is configured for a gain of +2. The input signal is terminated in 50  $\Omega$  and the

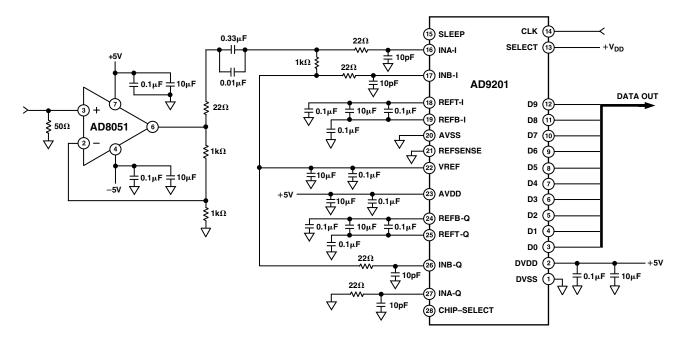


Figure 17. AD8051 Driving an AD9201, a 10-Bit 20 MSPS A/D Converter

output is 2 V p-p, which is the maximum input range of the AD9201. The 22  $\Omega$  series resistor limits the maximum current that flows and helps to lower the distortion of the A/D.

The AD9201 has differential inputs for each channel. These are designated the A and B inputs. The B inputs of each channel are connected to VREF (Pin 22), which supplies a positive reference of 2.5 V. Each of the B inputs has a small low-pass filter that also helps to reduce distortion.

The output of the op amp is ac-coupled into INA-I (Pin 16) via two parallel capacitors to provide good high frequency and low frequency coupling. The 1 k $\Omega$  resistor references the signal to VREF that is applied to INB-I. Thus, INA-I swings both positive and negative with respect to the bias voltage applied to INB-I.

With the sampling clock running at 20 MSPS, the A/D output was analyzed with a digital analyzer. Two input frequencies were used, 1 MHz and 9.5 MHz, which is just short of the Nyquist frequency. These signals were well filtered to minimize any harmonics.

Figure 18 shows the FFT response of the A/D for the case of a 1 MHz analog input. The SFDR is -71.66 dB and the A/D is producing 8.8 ENOB (effective number of bits). When the analog frequency was raised to 9.5 MHz, the SFDR was reduced to -60.18 dB and the A/D operated with 8.46 ENOBs as shown in Figure 19. The inclusion of the AD8051 in the circuit did not worsen the distortion performance of the AD9201.

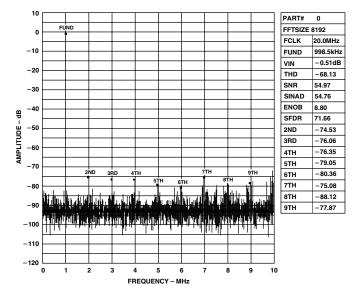


Figure 18. FFT Plot for AD8051 Driving the AD9201 at 1 MHz

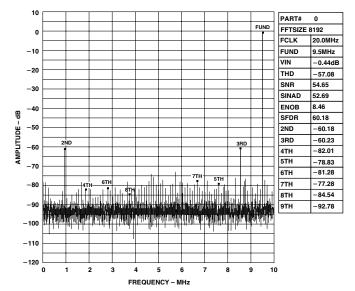
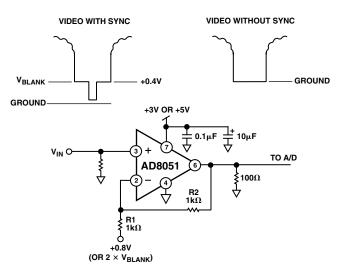


Figure 19. FFT Plot for AD8051 Driving the AD9201 at 9.5 MHz

#### Sync Stripper

Synchronizing pulses are sometimes carried on video signals so as not to require a separate channel to carry the synchronizing information. However, for some functions, such as A/D conversion, it is not desirable to have the sync pulses on the video signal. These pulses reduce the dynamic range of the video signal and do not provide any useful information for such a function.

A sync stripper removes the synchronizing pulses from a video signal while passing all the useful video information. Figure 20 shows a practical single-supply circuit that uses only a single AD8051. It is capable of directly driving a reverse terminated video line.



#### Figure 20. Sync Stripper

The video signal plus sync is applied to the noninverting input with the proper termination. The amplifier gain is set to 2 via the two 1 k $\Omega$  resistors in the feedback circuit. A bias voltage must be applied to R1 so that the input signal has the sync pulses stripped at the proper level.

The blanking level of the input video pulse is the desired place to remove the sync information. This level is multiplied by 2 by the amplifier. This level must be at ground at the output for the sync stripping action to take place. Since the gain of the amplifier from the input of R1 to the output is -1, a voltage equal to  $2 \times V_{BLANK}$  must be applied to make the blanking level come out at ground.

#### Single-Supply Composite Video Line Driver

Many composite video signals have their blanking level at ground and have video information that is both positive and negative. Such signals require dual-supply amplifiers to pass them. However by ac level shifting, a single-supply amplifier can be used to pass these signals. The following complications may arise from such techniques.

Signals of bounded peak-to-peak amplitude that vary in duty cycle require larger dynamic swing capacity than their (bounded) peak-to-peak amplitude after they are ac-coupled. As a worst case, the dynamic signal swing will approach twice the peak-to-peak value. The two conditions that define the maximum dynamic swing requirements are a signal that is mostly low but goes high with a duty cycle that is a small fraction of a percent, and the other extreme defined by the opposite condition.

The worst case of composite video is not quite this demanding. One bounding condition is a signal that is mostly black for an entire frame but has a white (full amplitude) minimum width spike at least once in a frame.

The other extreme is for a full white video signal. The blanking intervals and sync tips of such a signal have negative-going excursions in compliance with the composite video specifications. The combination of horizontal and vertical blanking intervals limit such a signal to being at the highest (white) level for a maximum of about 75% of the time.

As a result of the duty cycles between the two extremes presented above, a 1 V p-p composite video signal that is multiplied by a gain of +2 requires about 3.2 V p-p of dynamic voltage swing at the output for an op amp to pass a composite video signal of arbitrarily varying duty cycle without distortion.

Some circuits use a sync tip clamp to hold the sync tips at a relatively constant level to lower the amount of dynamic signal swing required. However, these circuits can have artifacts such as sync tip compression unless they are driven by a source with a very low output impedance. The AD8051/AD8052/AD8054 have adequate signal swing when running on a single 5 V supply to handle an ac-coupled composite video signal.

The input to the circuit in Figure 21 is a standard composite (1 V p-p) video signal that has the blanking level at ground. The input network level shifts the video signal by means of ac coupling. The noninverting input of the op amp is biased to half of the supply voltage.

The feedback circuit provides unity gain for the dc-biasing of the input and provides a gain of 2 for any signals that are in the video bandwidth. The output is ac-coupled and terminated to drive the line.

The capacitor values were selected for providing minimum *tilt* or field time distortion of the video signal. These values would be required for video that is considered to be studio or broadcast quality. However, if a lower consumer grade of video, sometimes referred to as *consumer video*, is all that is desired, the values and the cost of the capacitors can be reduced by as much as a factor of five with minimum visible degradation in the picture.

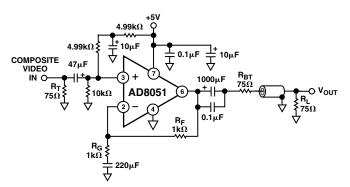
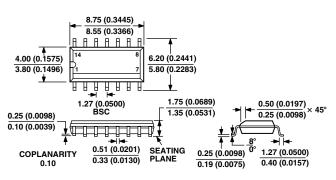


Figure 21. Single-Supply Composite Video Line Driver

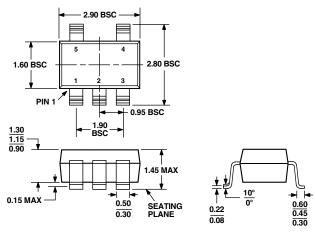
#### **OUTLINE DIMENSIONS**

14-Lead Standard Small Outline Package [SOIC] Narrow Body (RN-14) Dimensions shown in millimeters and (inches)



COMPLIANT TO JEDEC STANDARDS MS-012AB CONTROLLING DIMENSIONS ARE IN MILLIMETERS; INCH DIMENSIONS (IN PARENTHESES) ARE ROUNDED-OFF MILLIMETER EQUIVALENTS FOR REFERENCE ONLY AND ARE NOT APPROPRIATE FOR USE IN DESIGN 5-Lead Plastic Surface-Mount Package [SOT-23]

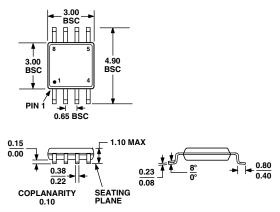
(RT-5) Dimensions shown in millimeters



COMPLIANT TO JEDEC STANDARDS MO-178AA

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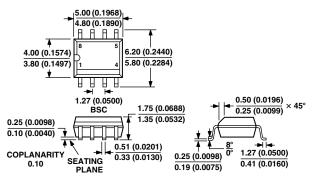
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COMPLIANT TO JEDEC STANDARDS MO-187AA

8-Lead Standard Small Outline Package [SOIC] Narrow Body (RN-8)

Dimensions shown in millimeters and (inches)

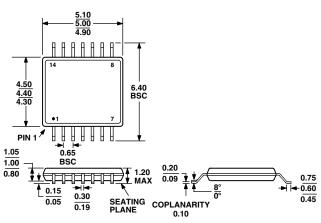


COMPLIANT TO JEDEC STANDARDS MS-012AA CONTROLLING DIMENSIONS ARE IN MILLIMETERS; INCH DIMENSIONS (IN PARENTHESES) ARE ROUNDED-OFF MILLIMETER EQUIVALENTS FOR REFERENCE ONLY AND ARE NOT APPROPRIATE FOR USE IN DESIGN

#### **OUTLINE DIMENSIONS**

#### 14-Lead Thin Shrink Small Outline Package [TSSOP] (RU-14)

Dimensions shown in millimeters



COMPLIANT TO JEDEC STANDARDS MO-153AB-1

# **Revision History**

Location	Page
2/03—Data Sheet changed from REV. C to REV. D.	
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Changes to ABSOLUTE MAXIMUM RATINGS	6
1/03—Data Sheet changed from REV. B to REV. C.	
Changes to GENERAL DESCRIPTION	1
Changes to PIN CONNECTIONS	1
Changes to SPECIFICATIONS	2
Changes to ABSOLUTE MAXIMUM RATINGS	9
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Changes to ORDERING GUIDE	
Updated OUTLINE DIMENSIONS	

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