

FAN73402 LED Backlight Driving Boost Switch

Features

- Single-Channel Boost LED Switch
- Internal Power MOSFET for PWM Dimming: R_{DS(ON)}=1.0Ω at V_{GS}=10V, BV_{DSS}=200V
- Current-Mode PWM Control
- Internal Programmable Slope Compensation
- Wide Supply Voltage Range: 10V to 35V
- LED Current Regulation: ±1%
- Programmable Switching Frequency
- Analog and PWM Dimming
- Wide Dimming Ratio: On Time=10µs to DC
- Cycle-by-Cycle Current Limiting
- Thermal Shutdown: 150°C
- Open-LED Protection (OLP)
- Over-Voltage Protection (OVP)
- Over-Current Protection (OCP)
- Error Flag Generation (for External Load Switch)
- Internal Soft-Start
- 16-Lead SOIC Package

Applications

- LED Backlight for LCD TV
- LED Backlight for LCD Monitor
- LED Lighting

Description

The FAN73402 is a single-channel boost controller that integrates an N-channel power MOSFET for PWM dimming using Fairchild's proprietary planar Double-diffused MOSFET (DMOS) technology.

The IC operates as a constant-current source for driving high-current LEDs.

It uses Current Mode control with programmable slope compensation to prevent subharmonic oscillation. The IC provides protections including: open-LED protection, over-voltage protection, and direct-short protection for high system reliability.

The IC internally generates a FAULT signal with delay if an abnormal LED string condition occurs. PWM dimming and analog dimming functions can be implemented independently. Internal soft-start prevents inrush current flowing into output capacitor at startup.



Ordering	Information
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Part Number	Operating Temperature Range	Package	Packing Method
FAN73402MX	-40°C to +125°C	16-Lead, Small-Outline Integrated Circuit (SOIC)	Tape & Reel



FAN73402 — LED Backlight Driving Boost Switch



Pin Definitions

Pin #	Name	Description		
1	VCC	This pin is the supply voltage of the IC.		
2	DRV	This pin is the gate drive signal of the boost switch.		
3	GND	This pin is the ground of the IC.		
4	CS	This pin is for sensing the current flowing through an external MOSFET. It includes a built-ir 300ns blanking time. The peak of the current flowing through the MOSFET is limited to this pin voltage. Slope compensation of the boost controller can be programmed through the series resistor of this pin.		
5	REF	This pin is the 5V reference voltage pin. Maximum current capability is 3mA.		
6	FAULT	This pin is for indicating the fault signal. This pin is connected to the open drain. When OLP protection is occurred, the FAULT pin is pulled HIGH.		
7	RT	Dscillator frequency set of the boost switch (50kHz ~ 300kHz).		
8	SENSE	This pin is for sensing the current flowing through the LEDs. A sensing resistor is connected from this pin to ground. This pin is connected to the negative input of the internal error amplifier.		
9, 10	DRAIN	Drain pin of PWM dimming power MOSFET.		
12	ENA	Enable input pin. If voltage of this pin is higher than 1.22V, the IC starts to operate. If the voltage of this pin is lower than 1.15V, the IC stops operating.		
13	OVP	Over-voltage protection input pin. Output voltage of the boost circuit is connected to this pin through a resistor divider circuit. If this pin voltage is higher than 3V, OVP is triggered.		
14	CMP	his pin is the error amplifier output. Typically, a compensation capacitor and resistor are onnected to this pin from the ground.		
15	ADIM	This pin is for setting the current flowing through the LEDs. This pin is connected to the positive inputs of the internal error amplifier. Linear voltage range of ADIM is 0.3V~3.0V.		
16	BDIM	This pin is for the burst dimming signal. If this pin voltage is HIGH, the internal dimming MOSFET is turned on. If this pin voltage is LOW, the dimming MOSFET is turned off.		

Note:

1. Pin 11 is a "No Connect" pin (not shown in Figure 2).

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Absolute Maximum Ratings

Stresses exceeding the absolute maximum ratings may damage the device. The device may not function or be operable above the recommended operating conditions and stressing the parts to these levels is not recommended. In addition, extended exposure to stresses above the recommended operating conditions may affect device reliability. The absolute maximum ratings are stress ratings only. $T_A=25^{\circ}C$ unless otherwise specified.

Symbol	Parameter	Min.	Max.	Unit
V _{CC}	Supply Voltage	10	35	V
T _A	Operating Temperature Range	-40	+125	°C
TJ	Junction Temperature		+150	°C
T _{STG}	Storage Temperature Range	-65	+150	°C
θ _{JA}	Thermal Resistance Junction-to-Ambient ^(2,3)		120	°C/W
PD	Power Dissipation		0.9	W

Notes:

2. Thermal resistance test board; size 76.2mm x 114.3mm x 1.6mm (1S0P); JEDEC standard: JESD51-2, JESD51-3.

3. Assume no ambient airflow.

Pin Breakdown Voltage

Pin #	Name	Value	Unit
1	VCC	35	V
2	DRV	20	V
3	GND		V
4	CS	6	V
5	REF	6	V
6	FAULT	35	V
7	RT	6	V
8	SENSE	6	V

Pin #	Name	Value	Unit
9	DRAIN	200	V
10	DRAIN	200	V
12	ENA	6	V
13	OVP	6	V
14	CMP	6	V
15	ADIM	6	V
16	BDIM	6	V

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Electrical Characteristics

For typical values, $T_A = 25^{\circ}C$ and $V_{CC} = 15V$ unless otherwise specified. Specifications to $-40^{\circ}C \sim 125^{\circ}C$ are guaranteed by design based on final characterization results.

Symbol	Parameter	Condition	Min.	Тур.	Max.	Unit
Supply Volt	age Section					
V _{CC}	Input DC Supply Voltage Range ⁽⁴⁾		10		35	V
I _{SD}	Shutdown Mode Supply Current	BDIM Connected to GND		2	4	mA
Under-Volta	age Lockout Section					
V _{th}	Start Threshold Voltage		8.3	9.0	9.7	V
V _{th,hys}	Start Threshold Voltage Hysteresis		0.5	1.0	1.5	V
I _{st}	Standby Current	V _{CC} =V _{th} -0.2		200	300	μA
ON/OFF Sec	ction					
Von	On-State Input Voltage		2		5	V
V _{OFF}	Off-State Input Voltage				0.8	V
Error Ampli	fier Section		1			
Gm	Error Amplifier Transconductance ⁽⁴⁾	V _{ADIM} =1V	100	300	500	µmho
A _{V_ro}	Error Amplifier Output impedance ⁽⁴⁾			20		MΩ
Av	Error Amplifier Open-Loop Gain ⁽⁴⁾			60		dB
Voffset	Input Offset Voltage	V _{ADIM} =1V	-10		10	mV
l _{sin}	CMP Sink Current	V _{ADIM} =1V, V _{SENSE} =2V	100	200	300	μA
l _{sur}	CMP Source Current	V _{ADIM} =1V, V _{SENSE} =0V	100	200	300	μA
V _{IDR}	Input Differential Voltage Range		0		3	V
Vo	Output Voltage Range		0.7		4.0	V
Oscillator S	Section		1			
		Minimum		50		
f _{osc}	Boost Oscillator Frequency	R _T =100kΩ	190	200	210	kHz
		Maximum		300		
D _{max}	Maximum Duty Cycle ⁽⁴⁾		86	90	94	%
Reference S	Section	1				
V _{REF}	5V Regulation Voltage		4.9	5.0	5.1	V
V _{REF,Line}	5V Line Regulation				25	mV
$V_{REF,Load}$	5V Load Regulation	0 <i5<3ma< td=""><td></td><td></td><td>25</td><td>mV</td></i5<3ma<>			25	mV
	ing Section		1		1	
V _{PDIM,L}	PWM Dimming Input Low Voltage				0.8	V
V _{PDIM,H}	PWM Dimming Input High Voltage		2	1	5	V
R _{PDIM}	PWM Dimming Pull-Down Resistance		100	160	220	kΩ
FET Sectior	n (for Dimming)	1				
BV _{DSS}	Drain-Source Breakdown Voltage ⁽⁴⁾	V _{CC} =0V, I _D =250µA	200			V
I _{DSS}	Zero-Gate-Voltage Drain Current ⁽⁴⁾	V _{DS} =250V, T _A =25°C		1	30	μA
R _{DS(ON)}	Drain-Source On-State Resistance	V _{GS} =10V, I _D =1A		0.7	1.0	Ω
CISS	Input Capacitance ⁽⁴⁾	V _{DS} =25V, V _{GS} =0V, f=1MHz		173	225	pF
C _{OSS}	Output Capacitance ⁽⁴⁾	V _{DS} =25V,V _{GS} =0V, f=1MHz		30	40	pF

Continued on the following page...

Symbol	Parameter	Condition	Min.	Тур.	Max.	Unit
	ion (Boost / Dimming)	Condition		Typ.	max.	01110
V _{DRV}	Gate Output Voltage	V _{CC} =15V	10.8	11.8	12.8	V
Vuv	Gate Output Voltage Before Startup		-0.5		0.5	V
I _{dsur}	Gate Output Drive-Source Current ⁽⁴⁾		80	180	280	mA
I _{dsin}	Gate Output Drive-Sink Current ⁽⁴⁾		80	180	280	mA
t _{rh}	Gate Output Rising Time (Boost) ⁽⁴⁾	C _L =2.0nF		200		ns
t _{fl}	Gate Output Falling Time (Boost) ⁽⁴⁾	C _L =2.0nF		120		ns
Current Sen				1	<u> </u>	
t _{blank}	Leading-Edge Blanking ⁽⁴⁾		150	300	450	ns
t _{delay,cl}	Delay to Output of Current-Limit Comparator ⁽⁴⁾				180	ns
V _{offset,clc}	Offset Voltage of Current-Limit Comparator ⁽⁴⁾		-20		20	mV
lope Comp	ensation Section					
I _{slope}	Ramp Generator Current		36	45	54	μA
R _{slope}	Slope Compensation Resistor ⁽⁴⁾			5		kΩ
Soft-Start Se	ection					
t _{ss}	Soft-Start Period ⁽⁴⁾	f _{osc} =200kHz		3		ms
Protection S	Section					
t _{d,ovp.tr}	Delay for Triggering Over-Voltage Protection ⁽⁴⁾		15	20	25	μs
t _{d,ovpr}	Delay for Releasing Over-Voltage Protection ⁽⁴⁾		10	14	18	μs
t _{d.ocp}	Delay for Over-Current Protection ⁽⁴⁾			1		μs
t _{AR}	Auto-Restart Time for Over-Current Protection ⁽⁴⁾	f _{osc} =200kHz		640		μs
t _{d,olpi}	Delay for Triggering Open-LED Protection ⁽⁴⁾		3	5	7	μs
t _{d,olp}	Delay for Open-LED Protection	f _{osc} =200kHz		40.96		ms
$V_{\text{th,ovp}}$	Over-Voltage Protection Threshold Voltage		2.85	3.00	3.15	V
V _{hys,ovp}	Over-Voltage Protection Voltage Hysteresis			0.1		V
$V_{\text{th.csocp}}$	Boost Switch Current-Limit Threshold Voltage		0.45	0.50	0.55	V
$V_{\text{th,ocp}}$	LED Over-Current Protection Threshold Voltage		1.4 (Min. Clamp)	4.0xV _A DIM	4.0 (Max. Clamp)	v
$V_{\text{th,olp}}$	Open-LED Protection Threshold Voltage ⁽⁴⁾		0.15	0.20	0.25	V
T _{SD}	Thermal Shutdown Temperature ⁽⁴⁾		140	150	160	°C

Note:

4. These parameters, although guaranteed, are not tested in production.

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FAN73402 — LED Backlight Driving Boost Switch









Functional Description

The FAN73402 operates as a constant-current source for driving high-current LEDs. It uses Current-Mode control with programmable slope compensation to prevent subharmonic oscillation.

The IC provides open-LED protection, over-voltage protection, and over-current protection for improved system reliability. The IC internally generates a FAULT OUT signal with a delay in case an abnormal LED string condition occurs. PWM dimming and analog dimming functions can be implemented independently. Internal soft-start prevents inrush current flowing into output capacitor at startup.

V_{cc} Under-Voltage Lockout (UVLO)

An internal regulator provides the regulated 5V used to power the IC. The Under-Voltage Lockout (UVLO) turns off the IC in the event of the voltage dropping below the specific threshold level. The UVLO circuit inhibits powering the IC until a voltage reference is established, up to predetermined threshold level.

Enable

Applying voltage higher than 1.22V (typical) to the ENA pin enables the IC. Applying voltage lower than 1.15V (typical) to the ENA pin disables the IC. If ENA pin voltage is higher than 1.22V (typical) and V_{CC} is higher than 9.0V (typical), the IC starts to supply the 5V reference voltage from V_{CC} .

Oscillator (Boost Switching Frequency)

Boost switching frequency is programmed by the value of the resistor connected from the RT pin to ground. RT pin voltage is set to 2V. The current through the RT pin resistor determines the boost switching frequency according to formula:

$$f_{OSC} = \frac{1}{(46.5 \times RT[k\Omega] + 350) \times 10^{-6}} [kHz]$$
(1)

Soft-Start Function at Startup

During initial startup, the switching device can be damaged due to the over-current coming from the input line by the negative control. This can result in the initial overshoot of the LED current. Therefore, during initial startup, the soft-start control gradually increases the duty cycle so that the output voltage can rise smoothly to control inrush current and overshoot.

FAN73402 adapts the soft-start function in the boost converter stage. During soft-start period, boost switch turn-on duty is limited by the clamped CMP voltage. The soft-start period is dependent on the boost switching frequency, which is determined by the RT resistor (Equation 1). Soft-start period is set to be cumulative time when the BDIM (PWM dimming) signal is HIGH:

$$t_{\rm SS} = 600 / f_{\rm OSC} [seconds]$$
(2)



Figure 26. Soft-Start Waveforms

LED Current Setting

During the boost converter operating periods, the output LED current can be set by equation:

$$I_{LED} = \frac{ADIM(V)}{R_{SENSE} + 60m\Omega}$$
(3)

where ADIM(V) is ADIM pin applied voltage and, $R_{\mbox{\scriptsize SENSE}}$ is the sensing resistor value.

Note:

 An additional 60mΩ comes from an internal wire bonding resistor. To calculate LED current precisely, consider the wire bonding resistor.

Analog Dimming and PWM Dimming

Analog dimming (ADIM) is achieved by varying the voltage level at the ADIM pin. This can be implemented either with a potentiometer from the VREF pin or from an external voltage source and a resistor divider circuit. The ADIM voltage level is adjusted to be the same as the feedback level (V_{SENSE}). A V_{ADIM} range from 0.3V to 3V is recommended.

PWM dimming (BDIM) helps achieve a fast PWM dimming response in spite of the shortcomings of the boost converter. The PWM dimming signal controls three nodes in the IC: gate signal to the switching FET, gate signal to the dimming FET, and output connection of the transconductance amplifier. When the PWM dimming signal is HIGH, the gates of the switching FET and dimming FET are enabled. At the same time, the output of the transconductance op-amp is connected to the compensation network. This allows the boost converter to operate normally.

Dynamic Contrast Ratio

The Dynamic Contrast Ratio (DCR) means the maximum contrast ratio achievable by adjusting the amount of light (dimming) of the screen using the backlight during an extremely short period of time. FAN73402 can normally drive the LED backlight under 0.1% dimming duty cycle at 200Hz dimming frequency. Even operating at 5µs dimming MOSFET turn-on time and extremely low dimming duty, FAN73402 can operate LEDs with normal peak current level.

Internal Dimming MOSFET

A dimming MOSFET (200V N-channel MOSFET) is incorporated in the FAN73402. The power transistor is produced using Fairchild's proprietary, planar stripe, DMOS technology. This advanced technology is tailored to minimize on-state resistance ($R_{DS(on)}$ =1.0 Ω) to provide superior switching performance. This device is suited for high-efficiency SMPS and shows desirable thermal characteristic during operation. To prevent initial LED current overshoot at low V_{ADIM} levels, gate resistance of the internal dimming FET is designed as 5k Ω .

Feedback Loop Compensation

Stable closed-loop control can be accomplished by connecting a compensation network between COMP and GND. The compensation needed to stabilize the converter can be a Type-I circuit (a simple integrator) or a Type-II circuit (and integrator with and additional pole-zero pair). The type of the compensation circuit required is dependent on the phase of the power stage at the crossover frequency.

FAN73402 adopts a Type-II compensator circuit.

Programmed Current Control

FAN73402 uses Current-Mode control. Current-Mode control loops: an outer feedback loop that senses output voltage (current) and delivers a DC control voltage to an inner feedback loop, which senses the peak current of the inductor and keeps it constant on a pulse-by-pulse basis. One of the advantages of the Current-Mode control is line/load regulation, which is corrected instantaneously against line voltage changes without the delay of an error amplifier.

Programmable Slope Compensation

When the power converter operates in Continuous Conduction Mode (CCM), the current programmed controller is inherently unstable when duty is larger than 50%, regardless of the converter topology. The FAN73402 uses a Peak-Current-Mode control scheme with programmable slope compensation and includes an internal transconductance amplifier to accurately control the output current over all line and load conditions.

An internal R_{slope} resistor (5k Ω) connected to sensing resistor, R_s , and an external resistor, R_1 , can control the slope of V_{SC} for the slope compensation. Although the normal operating mode of the power converter is DCM, the boost converter operates in CCM in the case of rapid LED current increase. As a result, slope compensation is an important feature.

The value of an external series resistor (R1) can be programmed. In normal DCM operation, $5k\Omega$ is recommended.



Figure 27. Slope Compensation

Cycle-by-Cycle Over-Current Protection

In boost topology, the switch can be damaged in abnormal conditions (inductor short, diode short, output short). It is always necessary to sense the switch current to protect against over-current failures. Switch failures due to excessive current can be prevented by limiting I_d .



Figure 28. Cycle-by-Cycle OCP Circuit

When the voltage drops at R_1 and R_s exceed a threshold of approximately 0.5V, the power MOSFET over-current function is triggered after minimum turn-on time or LEB time (300ns).

The peak voltage level at CS terminal:

$$V_{cs \text{ peak}} = 45\mu \times (R_1 + R_s) \times DT_s + I_d \times R_s$$
(4)

Choose the boost switch current-sensing resistor (R_{CS}):

$$R_{\rm CS} \ge \frac{0.25}{I_{\rm L \ peak}} \tag{5}$$

Open-LED Protection (OLP)

After the first PWM dimming-HIGH signal, the feedback sensing resistor (R_{SENSE}) starts sensing the LED current. If the feedback voltage of the SENSE pin drops below 0.2V, the OLP triggers to generate an error flag signal. Because OLP can be detected only in PWM dimming-HIGH; if OLP detecting time is over 5µs, PWM dimming signal is pulled HIGH internally regardless of external dimming signal. If OLP signal continues over blanking time, an error flag signal is triggered.

OLP blanking time is dependent on the boost switch frequency, per Equation 6. FAULT OUT signal is made through the FAULT pin, which needs to be connected 5V reference voltage through a pull-up resistor. In normal operation, the FAULT pin voltage is pulled down to ground. In OLP condition, the FAULT pin voltage is pulled HIGH.

$$t_{d.olp} = 8192 / f_{OSC} [seconds]$$

In system operation, OLP is triggered in only direct-short condition. Direct short means that some point of the LED string is shorted to set ground. In direct-short condition, the boost controller cannot control the LED current and a large current flows into the LED string directly from input power. To prevent this abnormal condition, the FAULT signal is used to turn off input power or the total system. FAULT signal is only triggered in OLP condition.



Note:

 In LED-open load condition, OVP is triggered ahead of OLP.

Over-Voltage Protection (OVP)

Over-voltage protection is triggered when the voltage of the external output voltage reaches 3V. After triggering OVP, the dimming switch and boost switch are turned off. The protection signal is recovered when the output voltage divider is below 2.9V.





LED Over-Current Protection (OCP)

(6)

The primary purpose of the over-current protection function is to protect the internal dimming MOSFET from excessive current. The OCP is triggered when the feedback voltage meets the clamping level $(1.4V \sim 4V)$ of the ADIM voltage x4. At 1µs delay after the OCP is triggered, the IC turns off both the boost FET and dimming FET and restarts the gate signal every tar automatically. t_{AR} can be calculated as:

 $t_{AR} = 128 / f_{OSC} [seconds]$ (7)

When VADIM=0.3V (VADIMX4=1.2V).

OCP threshold level is set to 1.4V.

OCP is triggered at feedback voltage level = 1.4V.



Figure 32. OCP Waveforms at V_{ADIM}=0.3V

When V_{ADIM} =0.8V ($V_{ADIM}x4$ =3.2V). OCP threshold level is set to 3.2V.

OCP is triggered at V_{SENSE} = 3.2V.



Figure 33. OCP Waveforms at V_{ADIM}=0.8V

When V_{ADIM} =1.2V ($V_{ADIM}x4$ =4.8V). OCP threshold level is set to 4.0V. OCP is triggered at V_{SENSE} = 4.0V.



Figure 34. OCP Waveforms at V_{ADIM}=1.2V

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Typical Application Circuit (Boost Topology for LED Backlight)				
Application	Input Voltage Range	Rated Output Power	Output Current (Rated Voltage)	LED
LED Backlight TV	$90V_{DC}\pm10\%$		250mA (160V)	48-LEDs/1-String

Features

- High Efficiency
- Constant Current Boost Converters
- High-Voltage, High-Current LED Driving

Typical Application Circuit





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Rev. 162

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