

LM431A

Adjustable Precision Zener Shunt Regulator

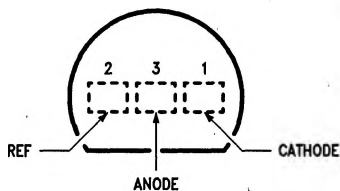
General Description

The LM431A is a 3-terminal adjustable shunt regulator with guaranteed temperature stability over the entire temperature range of operation. The output voltage may be set at any level greater than 2.5V (V_{REF}) up to 36V merely by selecting two external resistors that act as a voltage divided network. Due to the sharp turn-on characteristics this device is an excellent replacement for many zener diode applications.

Features

- Average temperature coefficient 50 ppm/°C
- Temperature compensated for operation over the full temperature range
- Programmable output voltage
- Fast turn-on response
- Low output noise

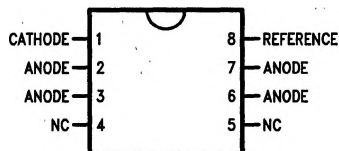
Connection Diagrams



Top View

Order Number LM431ACZ or LM431AIZ
See NS Package Number Z03A

TL/H/10055-1



Top View

Order Number LM431ACM or LM431AIM
See NS Package Number M08A

TL/H/10055-2

Absolute Maximum Ratings

If Military/Aerospace specified devices are required, please contact the National Semiconductor Sales Office/Distributors for availability and specifications.

Storage Temperature Range -65°C to $+150^{\circ}\text{C}$

Operating Temperature Range

Industrial (LM431AI) -40°C to $+85^{\circ}\text{C}$

Commercial (LM431AC) 0°C to $+70^{\circ}\text{C}$

Lead Temperature

TO-92 Package/SO-8 Package

(Soldering, 10 sec.) 265°C

Internal Power Dissipation (Notes 1, 2)

TO-92 Package 0.78W

SO-8 Package 0.81W

Cathode Voltage 37V

Continuous Cathode Current $-10\text{ mA to } +150\text{ mA}$

Reference Voltage -0.5V

Reference Input Current 10 mA

Operating Conditions **Min** **Max**

Cathode Voltage V_{REF} 37V

Cathode Current 1.0 mA 100 mA

Note 1: $T_J \text{ Max} = 150^{\circ}\text{C}$.

Note 2: Ratings apply to ambient temperature at 25°C . Above this temperature, derate the TO-92 at $6.2\text{ mW}/^{\circ}\text{C}$, and the SO-8 at $6.5\text{ mW}/^{\circ}\text{C}$.

LM431A

Electrical Characteristics $T_A = 25^{\circ}\text{C}$ unless otherwise specified

Symbol	Parameter	Conditions	Min	Typ	Max	Units
V_{REF}	Reference Voltage	$V_Z = V_{\text{REF}}, I_1 = 10\text{ mA}$ (Figure 1)	2.440	2.495	2.550	V
V_{DEV}	Deviation of Reference Input Voltage Over Temperature (Note 3)	$V_Z = V_{\text{REF}}, I_1 = 10\text{ mA}$, $T_A = \text{Full Range}$ (Figure 1)		8.0	17	mV
$\frac{\Delta V_{\text{REF}}}{\Delta V_Z}$	Ratio of the Change in Reference Voltage to the Change in Cathode Voltage	$I_Z = 10\text{ mA}$ (Figure 2)				mV/V
		V_Z from V_{REF} to 10V		-1.4	-2.7	
		V_Z from 10V to 36V		-1.0	-2.0	
I_{REF}	Reference Input Current	$R_1 = 10\text{ k}\Omega, R_2 = \infty$, $I_1 = 10\text{ mA}$ (Figure 2)		2.0	4.0	μA
αI_{REF}	Deviation of Reference Input Current over Temperature	$R_1 = 10\text{ k}\Omega, R_2 = \infty$, $I_1 = 10\text{ mA}$, $T_A = \text{Full Range}$ (Figure 2)		0.4	1.2	μA
$I_Z(\text{MIN})$	Minimum Cathode Current for Regulation	$V_Z = V_{\text{REF}}$ (Figure 1)		0.4	1.0	mA
$I_Z(\text{OFF})$	Off-State Current	$V_Z = 36\text{V}, V_{\text{REF}} = 0\text{V}$ (Figure 3)		0.3	1.0	μA
r_Z	Dynamic Output Impedance (Note 4)	$V_Z = V_{\text{REF}}$, Frequency = 0 Hz (Figure 1)			0.75	Ω

Note 3: Deviation of reference input voltage, V_{DEV} , is defined as the maximum variation of the reference input voltage over the full temperature range.

The average temperature coefficient of the reference input voltage, αV_{REF} , is defined as:

$$\alpha V_{\text{REF}} \frac{\text{ppm}}{^{\circ}\text{C}} = \frac{\pm \left[\frac{V_{\text{MAX}} - V_{\text{MIN}}}{V_{\text{REF}}(\text{at } 25^{\circ}\text{C})} \right] 10^6}{T_2 - T_1} = \frac{\pm \left[\frac{V_{\text{DEV}}}{V_{\text{REF}}(\text{at } 25^{\circ}\text{C})} \right] 10^6}{T_2 - T_1}$$

Where:

$T_2 - T_1$ = full temperature change.

αV_{REF} can be positive or negative depending on whether the slope is positive or negative.

Example: $V_{\text{DEV}} = 8.0\text{ mV}$, $V_{\text{REF}} = 2.495\text{ mV}$, $T_2 - T_1 = 70^{\circ}\text{C}$, slope is positive.

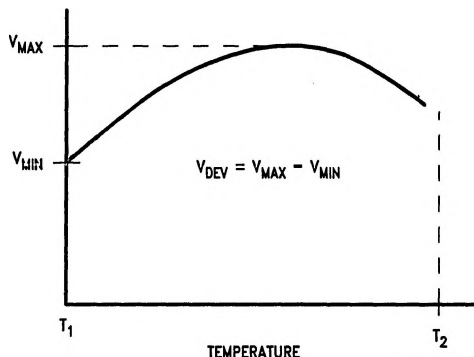
$$\alpha V_{\text{REF}} = \frac{\left[\frac{8.0\text{ mV}}{2.495\text{ mV}} \right] 10^6}{70^{\circ}\text{C}} = +46\text{ ppm}/^{\circ}\text{C}$$

Note 4: The dynamic output impedance, r_Z , is defined as:

$$r_Z = \frac{\Delta V_Z}{\Delta I_Z}$$

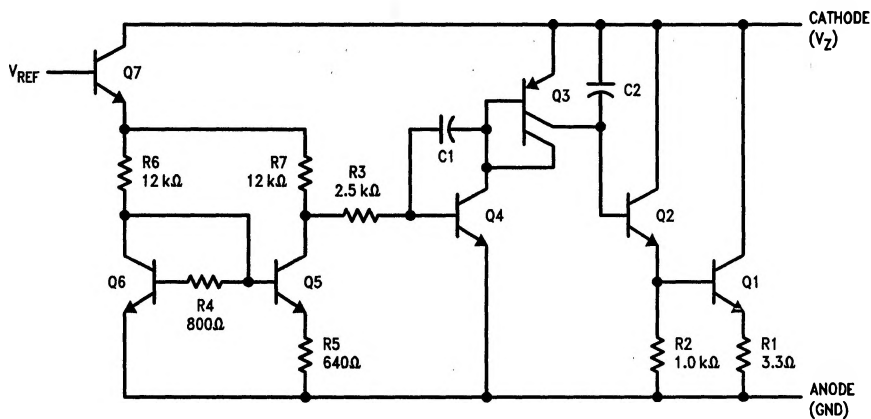
When the device is programmed with two external resistors, R_1 and R_2 , (see Figure 2), the dynamic output impedance of the overall circuit, r_Z , is defined as:

$$r_Z = \frac{\Delta V_Z}{\Delta I_Z} \approx \left[r_Z 1 + \frac{R_1}{R_2} \right]$$



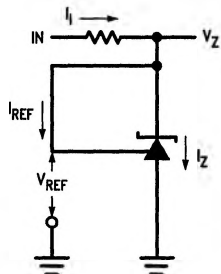
TL/H/10055-7

Equivalent Circuit

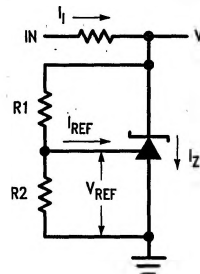


TL/H/10055-3

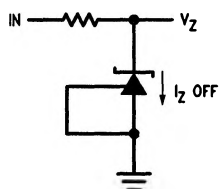
DC Test Circuits



TL/H/10055-4

FIGURE 1. Test Circuit for $V_Z = V_{REF}$ 

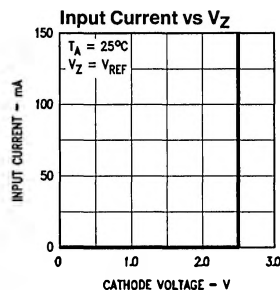
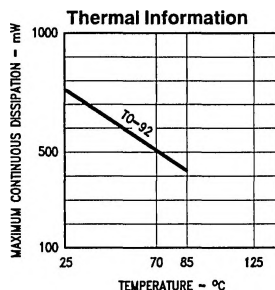
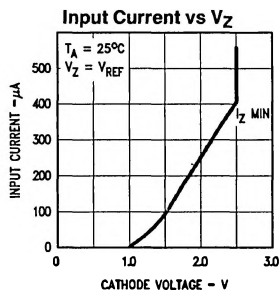
TL/H/10055-5

Note: $V_Z = V_{REF} (1 + R_1/R_2) + I_{REF} \cdot R_1$ FIGURE 2. Test Circuit for $V_Z > V_{REF}$ 

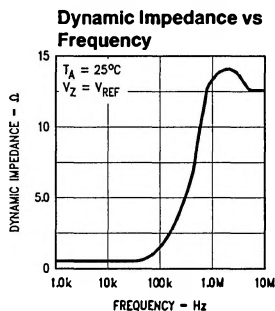
TL/H/10055-6

FIGURE 3. Test Circuit for Off-State Current

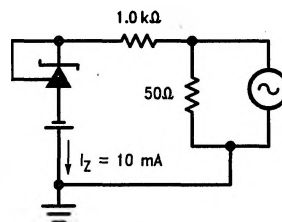
Typical Performance Characteristics



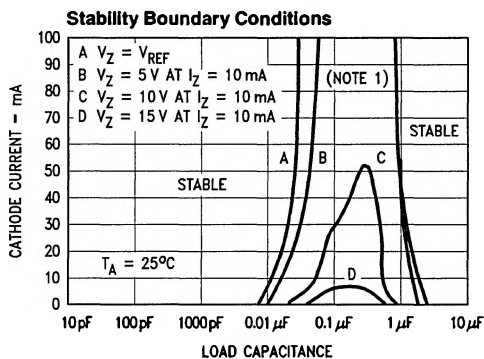
TL/H/10055-8



TL/H/10055-9



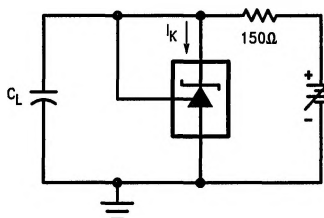
TL/H/10055-10



TL/H/10055-11

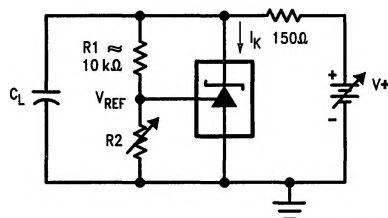
Note 1: The areas under the curves represent conditions that may cause the device to oscillate. For curves B, C, and D, R_2 and V^+ were adjusted to establish the initial V_Z and I_Z conditions with $C_L = 0$. V^+ and C_L were then adjusted to determine the ranges of stability.

Test Circuit for Curve A Above



TL/H/10055-12

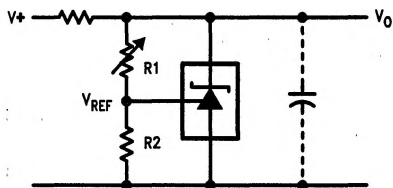
Test Circuit for Curves B, C and D Above



TL/H/10055-13

Typical Applications

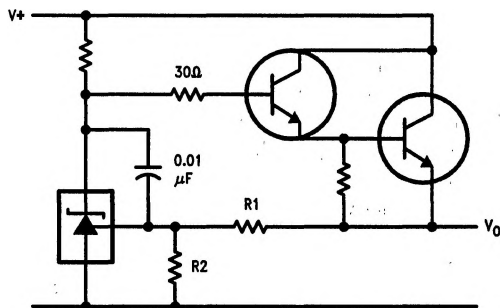
Shunt Regulator



TL/H/10055-14

$$V_O \approx \left(1 + \frac{R_1}{R_2}\right) V_{REF}$$

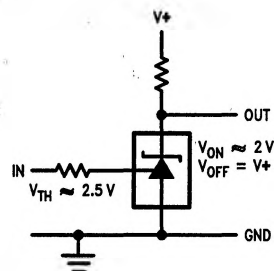
Series Regulator



TL/H/10055-16

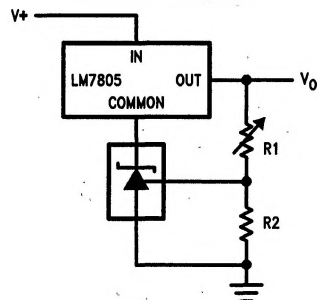
$$V_O \approx \left(1 + \frac{R_1}{R_2}\right) V_{REF}$$

Single Supply Comparator with Temperature Compensated Threshold



TL/H/10055-15

Output Control of a Three Terminal Fixed Regulator



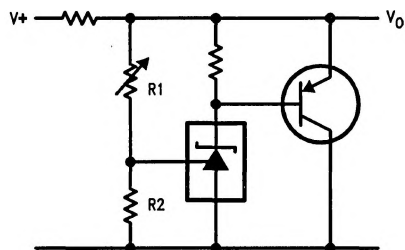
TL/H/10055-17

$$V_O = \left(1 + \frac{R_1}{R_2}\right) V_{REF}$$

$$V_{O\ MIN} = V_{REF} + 5V$$

Typical Applications (Continued)

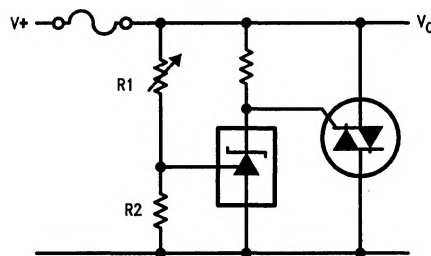
Higher Current Shunt Regulator



TL/H/10055-18

$$V_O = \left(1 + \frac{R_1}{R_2}\right) V_{REF}$$

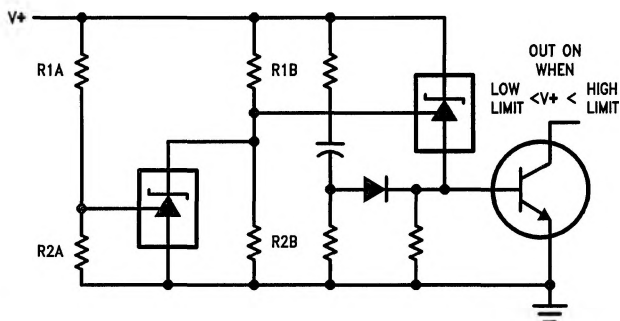
Crow Bar



TL/H/10055-19

$$V_{LIMIT} \approx \left(1 + \frac{R_1}{R_2}\right) V_{REF}$$

Over Voltage/Under Voltage Protection Circuit

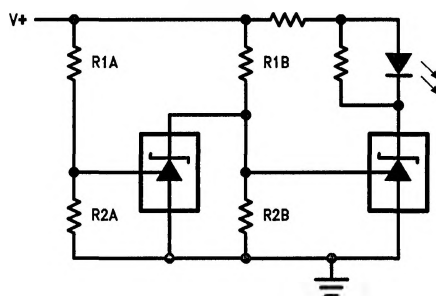


TL/H/10055-20

$$\text{LOW LIMIT} \approx V_{REF} \left(1 + \frac{R_{1B}}{R_{2B}}\right) + V_{BE}$$

$$\text{HIGH LIMIT} \approx V_{REF} \left(1 + \frac{R_{1A}}{R_{2A}}\right)$$

Voltage Monitor



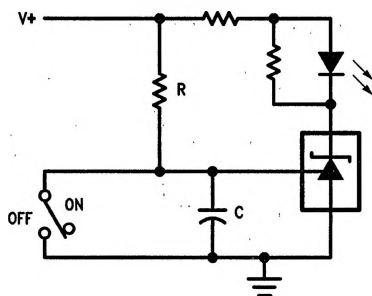
TL/H/10055-21

$$\text{LOW LIMIT} \approx V_{REF} \left(1 + \frac{R_{1B}}{R_{2B}}\right) \quad \text{LED ON WHEN LOW LIMIT} < V^+ < \text{HIGH LIMIT}$$

$$\text{HIGH LIMIT} \approx V_{REF} \left(1 + \frac{R_{1A}}{R_{2A}}\right)$$

Typical Applications (Continued)

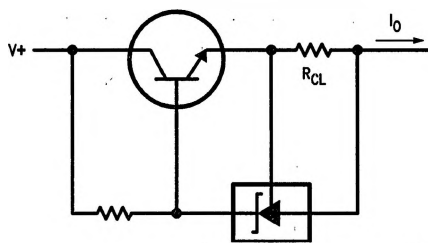
Delay Timer



TL/H/10055-22

$$\text{DELAY} = R \cdot C \cdot \ln \frac{V+}{(V+) - V_{\text{REF}}}$$

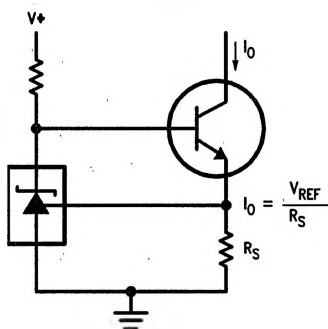
Current Limiter or Current Source



TL/H/10055-23

$$I_O = \frac{V_{\text{REF}}}{R_{\text{CL}}}$$

Constant Current Sink



TL/H/10055-24

$$I_O = \frac{V_{\text{REF}}}{R_S}$$