

High and low side driver configuration current

High Common Mode, Gain of 20, Precision Voltage Difference Amplifier

Check for Samples: LMP8275

Supply current 1 mA

Fuel injection control

Power management systems

APPLICATIONS

sensina

FEATURES

- Typical Values, T_A = 25°C
- Input offset voltage ±2 mV max
- TCVos ±30 µV/°C max
- CMRR 80 dB min
- Output voltage swing Rail-to-rail
- Bandwidth 80 kHz
- Operating temperature range (ambient) -40°C to 125°C
- Supply voltage 4.75V to 5.5V

DESCRIPTION

The LMP8275 is a fixed gain differential amplifier with a -2V to 16V input common mode voltage range and a supply voltage range of 4.75V to 5.5V. The LMP8275 is part of the LMPTM precision amplifier family which will detect, amplify and filter small differential signals in the presence of high common mode voltages. The gain is fixed at 20 and is adequate to drive an ADC to full scale in most cases. This gain is achieved in two stages, a preamplifier with a fixed gain of 10 and a second stage amplifier with a fixed gain of 2. The internal signal path between these two stages is brought out on two pins, A1 and A2, which provide a connection for a filter network.

The LMP8275 will function over an extended common mode input voltage range making the device suitable for applications with load dump events such as automotive systems.

Typical Application

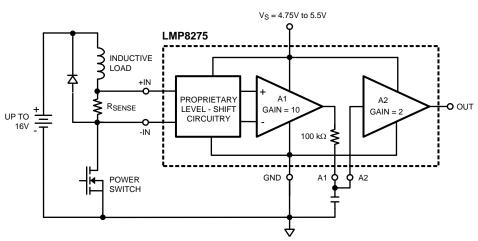


Figure 1. Low Side Current Sensing



These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

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ISTRUMENTS

EXAS

Absolute Maximum Ratings (1)

±4000V
±2000V
200V
5.75V
-7V to 45V
−65°C to +150°C
+150°C
235°C
260°C

(1) Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. Operating Ratings indicate conditions for which the device is intended to be functional, but specific performance is not guaranteed. For guaranteed specifications and the test conditions, see the Electrical Characteristics Tables.

(2) Human Body Model is 1.5 k Ω in series with 100 pF. Machine Model is 0 Ω in series with 200 pF.

(3) The maximum power dissipation is a function of $T_{J(MAX)}$, θ_{JA} , and T_A . The maximum allowable power dissipation at any ambient temperature is $P_D = (T_{J(MAX)} - T_A)/|\theta_{JA}|$. All numbers apply for packages soldered directly onto a PC board.

Operating Ratings ⁽¹⁾

Temperature Range						
Packaged Device ⁽²⁾	−40°C to +125°C					
Supply Voltage (V _S –GND)	4.75V to 5.5V					
Package Thermal Resistance ($\theta_{JA}^{(2)}$)						
8-Pin SOIC	190°C/W					

(1) Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. Operating Ratings indicate conditions for which the device is intended to be functional, but specific performance is not guaranteed. For guaranteed specifications and the test conditions, see the Electrical Characteristics Tables.

(2) The maximum power dissipation is a function of $T_{J(MAX)}$, θ_{JA} , and T_A . The maximum allowable power dissipation at any ambient temperature is $P_D = (T_{J(MAX)} - T_A)/|\theta_{JA}|$. All numbers apply for packages soldered directly onto a PC board.



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5V Electrical Characteristics ⁽¹⁾

Unless otherwise specified, all are limits guaranteed for $T_A = 25^{\circ}C$, $V_S = 5V$, GND = 0V, $-2V \le V_{CM} \le 16V$, $R_L = Open$. Boldface limits apply at the temperature extremes.

Symbol	Parameter	Conditions		Min	Тур (2)	Max	Units
V _{OS}	Input Offset Voltage				±0.25	±2.0	mV
TCV _{OS}	Input Offset Voltage Drift	$V_{CM} = V_S/2$	$25^{\circ}C \le T_A \le 125^{\circ}C$		±20 ±30		
			$-40^{\circ}C \le T_A \le 25^{\circ}C$		±20	±35	μV/°C
A2 I _B	Input Bias Current of A2	(3)			-20		fA
						±20	nA
I _S	Supply Current				1.0	1.2 1.4	mA
R _{CM}	Input Impedance Common Mode			160	200	240	kΩ
R _{DM}	Input Impedance Differential Mode			320	400	480	kΩ
CMVR	Input Common-Mode Voltage Range			-2		+16	V
DC	DC Common Mode Rejection Ratio	0°C ≤ T _A ≤ 125°C	$-2V \le V_{CM} \le 16V$	80	103		dB
CMRR		$-40^{\circ}C \le T_A \le 0^{\circ}C$	$-2V \le V_{CM} \le 16V$	77			
AC	AC Common Mode Rejection Ratio ⁽⁴⁾	$-2V \le V_{CM} \le 16V$	f = 1 kHz	80	95		dB
CMRR		$-2V \le V_{CM} \le 16V$	f = 10 kHz		78		
PSRR	Power Supply Rejection Ratio	4.75V ≤ V _S ≤ 5.5V		70	80		dB
R _{F-INT}	Filter Resistor			97	100	103	kΩ
TCR _{F-INT}	Filter Resistor Drift				±20		ppm/°C
A _V	Total Gain			19.8	20	20.2	V/V
	Gain Drift				±2	±25	ppm/°C
A _{V1}	A1 Gain			9.9	10	10.1	V/V
A _{V2}	A2 Gain			1.98	2.0	2.02	V/V
A1 V _{OUT}	A1 Output Voltage Swing		VOL		0.004	0.01	
			VOH	4.80	4.95		V
A2 V _{OUT}	A2 Output Voltage Swing	R_L = 100 k Ω on Output	VOL		0.007	0.02	- V
			VOH	4.80	4.99		
		R_L = 10 k Ω on Output VOL	VOL		0.03		- V
			VOH		4.95		
SR	Slew Rate (7)		- I-		0.7		V/µs
BW	Bandwidth				80		kHz
Noise	0.1 Hz to 10 Hz				5.7		μV _{PP}
	Spectral Density	f = 1 kHz			452		nV/√Hz

(1) Electrical table values apply only for factory testing conditions at the temperature indicated. Factory testing conditions result in very limited self-heating of the device.

Typical values represent the parametric norm at the time of characterization. (2)

(3) Positive current corresponds to current flowing into the device.
(4) AC Common Mode Signal is a 16 V_{PP} sine-wave (0V to 16V) at the given frequency
(5) For VOL, R_L is connected to V_S and for VOH, R_L is connected to GND.

(6) For this test input is driven from A1 stage.

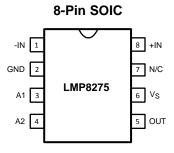
Slew rate is the average of the rising and falling slew rates. (7)

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Connection Diagram

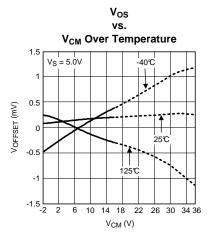




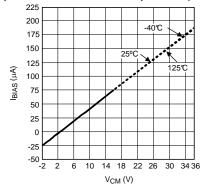


Typical Performance Characteristics

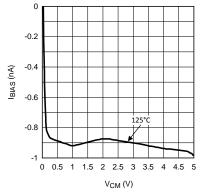
Unless otherwise specified: $T_A = 25^{\circ}C$, $V_S = 5V$, $V_{CM} = V_S/2$

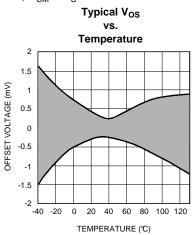






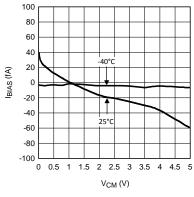




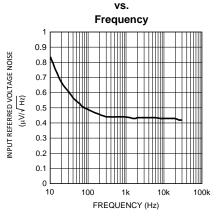


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Input Bias Current Over Temperature (A2 Input)



Input Referred Voltage Noise



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5.25

125

100k

1M

5.5

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Typical Performance Characteristics (continued) Unless otherwise specified: $T_A = 25^{\circ}C$, $V_S = 5V$, $V_{CM} = V_S/2$ v_{os} PSRR vs. vs. Frequency **Supply Voltage** 120 1 0.8 100 0.6 0.4 80 125°C 丶 PSRR (dB) Vos (mV) 0.2 0 60 25°C --0.2 40 -0.4 -40°C / -0.6 20 -0.8 0 -1 10 100 1k 10k 100k 4.75 5 FREQUENCY (Hz) $V_{S}(V)$ Gain Gain vs. vs. **Frequency Over Temperature Frequency Over Temperature** 30 30 20 20 10 10 GAIN (dB) GAIN (dB) 0 0 11111 -10 -10 Vs = 5V ∕_S = 5∨ 125 V_{OUT} = 500 mV $V_{OUT} = 3V$ -20 -20 10k 100k 10k 10 100 1k 1M 10 100 1k FREQUENCY (Hz) FREQUENCY (Hz) CMRR vs. **Filter Resistor** Frequency 30 120 25 100 PERCENTAGE (%) 20 80 CMRR (dB) 125 15 60 10 40 5 20 0 0

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96

98

100

RESISTOR VALUE (kΩ)

102

104

10

100

1k

FREQUENCY (Hz)

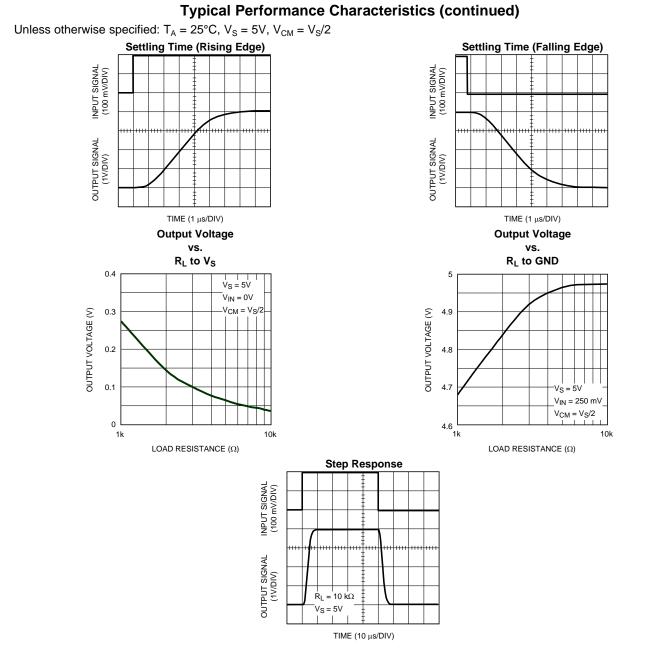
10k

100k





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Application Note

LMP8275

The LMP8275 is a single supply amplifiers with a fixed gain of 20 and a common mode voltage range of -2V to 16V. The fixed gain is achieved in two separate stages, a preamplifier with gain of +10 and a second stage amplifier with gain of +2. A block diagram of the LMP8275 is shown in Figure 3.

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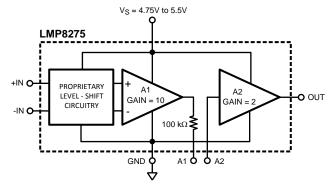


Figure 3. LMP8275

The overall offset of the LMP8275 is minimized by trimming amplifier A1. This is done in such a way that the output referred offset of A1 cancels the input referred offset of A2 or $10V_{OS1} = -V_{OS2}$.

Because of this offset voltage relationship, the offset of each individual amplifier stage may be more than the limit specified for the overall system in the datasheet tables. If the signal going from A1 to A2 is amplified or attenuated (by use of amplifiers and resistors), the overall LMP8275 offset will be affected as a result. Filtering the signal between A1 and A2 or simply connecting the two pins will not change the offset of the LMP8275.

Referencing input referred offset voltages, the following relationship holds:

$$\frac{(10V_{OS1}) + (V_{OS2})}{10} = V_{OS} (LMP8275)$$
(1)

If the signal on pin 3 is scaled, attenuated or amplified, by a factor **X**, then the offset of the overall system will become:

$$\frac{(10V_{OS1}) \times (X) + (V_{OS2})}{10 (X)} = V_{OS} (LMP8275)$$
(2)

POWER SUPPLY DECOUPLING

In order to decouple the LMP8275 from AC noise on the power supply, it is recommended to use a 0.1 μ F on the supply pin. It is best to use a 0.1 μ F capacitor in parallel with a 10 μ F capacitor. This will generate an AC path to ground for most frequency ranges and will greatly reduce the noise introduced by the power supply.

SECOND ORDER LOW PASS FILTER

The LMP8275 can be effectively used to build a second order Sallen-Key low pass filter. The general filter is shown in

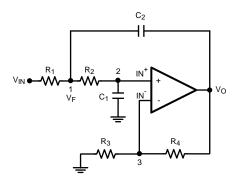


Figure 4. Second Order Low-Pass Filter



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With the general transfer function:

$$\frac{V_{O}}{V_{IN}} = \frac{K}{M - KN}$$

Where

$$\begin{split} \mathsf{M} &= \mathsf{s}^2 \mathsf{C}_1 \mathsf{C}_2 \mathsf{R}_1 \mathsf{R}_2 + \mathsf{s} (\mathsf{R}_1 \mathsf{C}_1 + \mathsf{R}_1 \mathsf{C}_2 + \mathsf{C}_1 \mathsf{R}_2) + 1 \\ \mathsf{N} &= \mathsf{s} \mathsf{C}_2 \mathsf{R}_1 \end{split}$$

and

$$\frac{1}{K} = \frac{1}{A_{VOL}} + \frac{R_3}{R_3 + R_4}$$

(5)

(3)

(4)

K represents the sum of DC closed loop gain and the non-ideal behavior of the operational amplifier. Assuming ideal behavior, the equation for K reduces simply to the DC gain, which is +2 for the LMP8275.

The LMP8275 can be used to realize this configuration as shown in Figure 5:

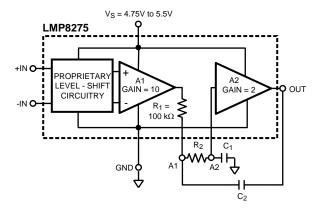


Figure 5. Low-Pass Filter With LMP8275

Assuming ideal behavior, the equation for K reduces simply to the DC gain, which is set for +2 for the LMP8270. Using Equation 3, the filter parameters can be calculated as follows:

$$\omega_{0} = \frac{1}{\sqrt{R_{1}R_{2}C_{1}C_{2}}}$$
$$f_{c} = \frac{1}{2\pi\sqrt{R_{1}R_{2}C_{1}C_{2}}}$$
$$\sqrt{R_{1}R_{2}C_{1}C_{2}}$$

$$Q = \frac{\sqrt{R_1 R_2 C_1 C_2}}{R_1 C_1 + R_2 C_1 + (1 - K) R_1 C_2}$$

(6)

for the LMP8275, $R_1 = 100 \text{ k}\Omega$. Setting $R_1 = R_2$ and $C_1 = C_2$ results in a low pass filter with Q = 1. Since the values of resistors are predetermined, the corner frequency of this implementation of the filter depends on the capacitor values.

GAINS OTHER THAN 20

THe LMP8275 has an internal gain of +20; however this gain can be modified. The signal path between the two amplifiers is available as external pins.

GAINS LESS THAN 20

Figure 6 shows the configuration used to reduce the LMP8275 gain.

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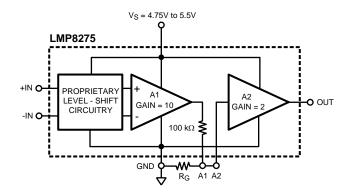


Figure 6. Gains Less Than 20

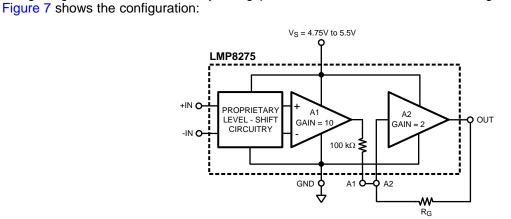
Where:

$$\text{GAIN (NEW)} = \frac{20 \text{ R}_{\text{G}}}{\text{R}_{\text{C}} + 100 \text{ k}\Omega}$$

and

$$R_{G} = (100 \text{ k}\Omega) \frac{\text{GAIN (NEW)}}{20 - \text{GAIN (NEW)}}$$

GAINS GREATER THAN 20



A higher gain can be achieved by using positive feedback on the second stage amplifier, A2, of LMP8275.

Figure 7. Gains Greater Than 20

The total gain is given by:

$$\text{GAIN (NEW)} = \frac{20 \text{ R}_{\text{G}}}{\text{R}_{\text{G}} - 100 \text{ k}\Omega}$$

Which can be rearranged to calculate R_G:

$$R_{G} = (100 \text{ k}\Omega) \frac{\text{GAIN (NEW)}}{\text{GAIN (NEW)} - 20}$$

(10)

The inverting gain of the second amplifier is set at 2, giving the total system a gain of 20. The non-inverting gain which is achieved through positive gain can be less than or equal to this gain without any issues. This implies a total gain of 40 or less is easily achievable. Once the positive gain surpasses the negative gain, the system might oscillate.

(7)

(8)

(9)

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As the value of gain resistor, R_G , approaches that of the internal 100 k Ω resistor, maintaining gain accuracy will become more challenging. This is because Gain (new) is inversely proportional to $(R_G-100 \ k\Omega)$, see Equation 9 . As $R_G \rightarrow 100 \ k\Omega$, the denominator of Equation 9 gets smaller. This smaller value will be comparable to the tolerance of the 100 $k\Omega$ resistor and R_G and hence the gain will be dominated by accuracy level of these resistors and the gain tolerance will be determined by the tolerance of the external resistor used for R_G and the 3% tolerance of the internal 100 $k\Omega$ resistor.

CURRENT LOOP RECEIVER

Many types of process control instrumentation use 4 to 20 mA transmitters to transmit the sensor's analog value to a central control room. The LMP8275 can be used as a current loop receiver as shown in Figure 8.

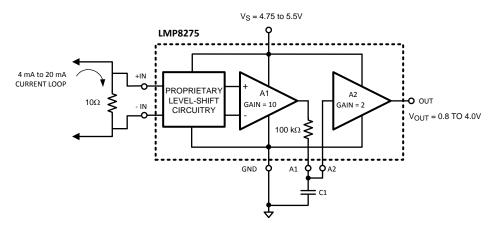


Figure 8. Current Loop Receiver

HIGH SIDE CURRENT SENSING

High side current measurement requires a differential amplifier with gain. Here the DC voltage source represent a common mode voltage with the +IN input at the supply voltage and the -IN input very close to the supply voltage. The LMP8275 can be used with a common mode voltage, V_{DC} in this case, of up to 16V.

The LMP8275 can be used for high side current sensing. The large common mode voltage range of this device allows it to sense signals outside of its supply voltage range. Also, the LMP8275 has very high CMRR, which enables it to sense very small signals in the presence of larger common mode signals. The system in Figure 9 couples these two characteristics of the LMP8275 in an automotive application. The signal through R_{S1} is detected and amplified by the LMP8275 in the presence of a common mode signal of up to 16V with the highest accuracy.



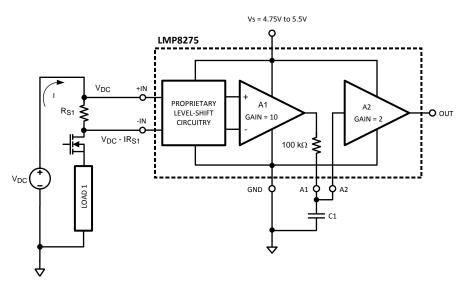


Figure 9. High Side Current Sensing

LOW SIDE CURRENT SENSING

Low side current measurements can cause a problem for operational amplifiers by exceeding the negative common mode voltage limit of the device. In Figure 10, the load current is returning to the power source through a common connection that has a parasitic resistance. The voltage drop across the parasitic resistances can cause the ground connection of the measurement circuits to be at a positive voltage with respect to the common side of the sense resistor. This will result in one or both of the inputs being negative with respect to the measurement circuit's ground. The LMP8275 has a wide input common mode voltage range of -2V to 16V and will function in this condition.

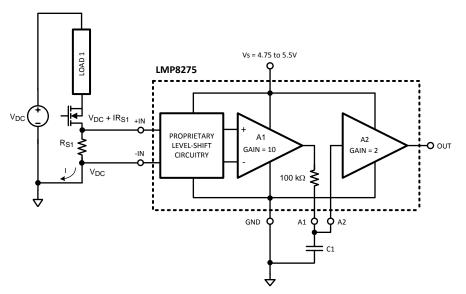


Figure 10. Low Side Current Sensing

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