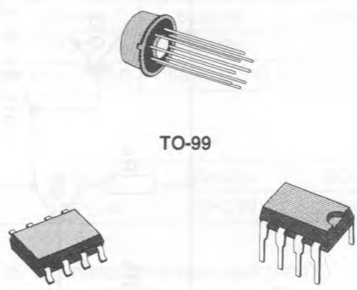
LS204

HIGH PERFORMANCE DUAL OPERATIONAL AMPLIFIER

- SINGLE OR SPLIT SUPPLY OPERATION
- LOW POWER CONSUMPTION
- SHORT CIRCUIT PROTECTION
- LOW DISTORTION, LOW NOISE
- HIGH GAIN-BANDWIDTH PRODUCT
- HIGH CHANNEL SEPARATION



TO-99

SO-8J

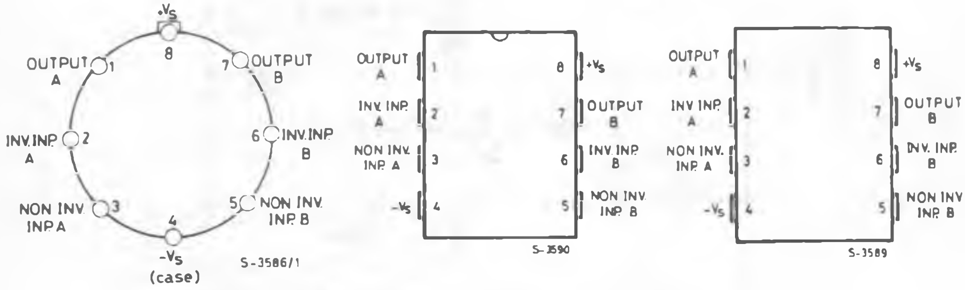
MINIDIP
(Plastic)

DESCRIPTION

The LS204 is a high performance dual operational amplifier with frequency and phase compensation built into the chip. The internal phase compensation allows stable operation as voltage follower in spite of its high gain-bandwidth products.

The circuit presents very stable electrical characteristics over the entire supply voltage range, and it particularly intended for professional and telecom applications (active filters, etc).

PIN CONNECTIONS (top views)

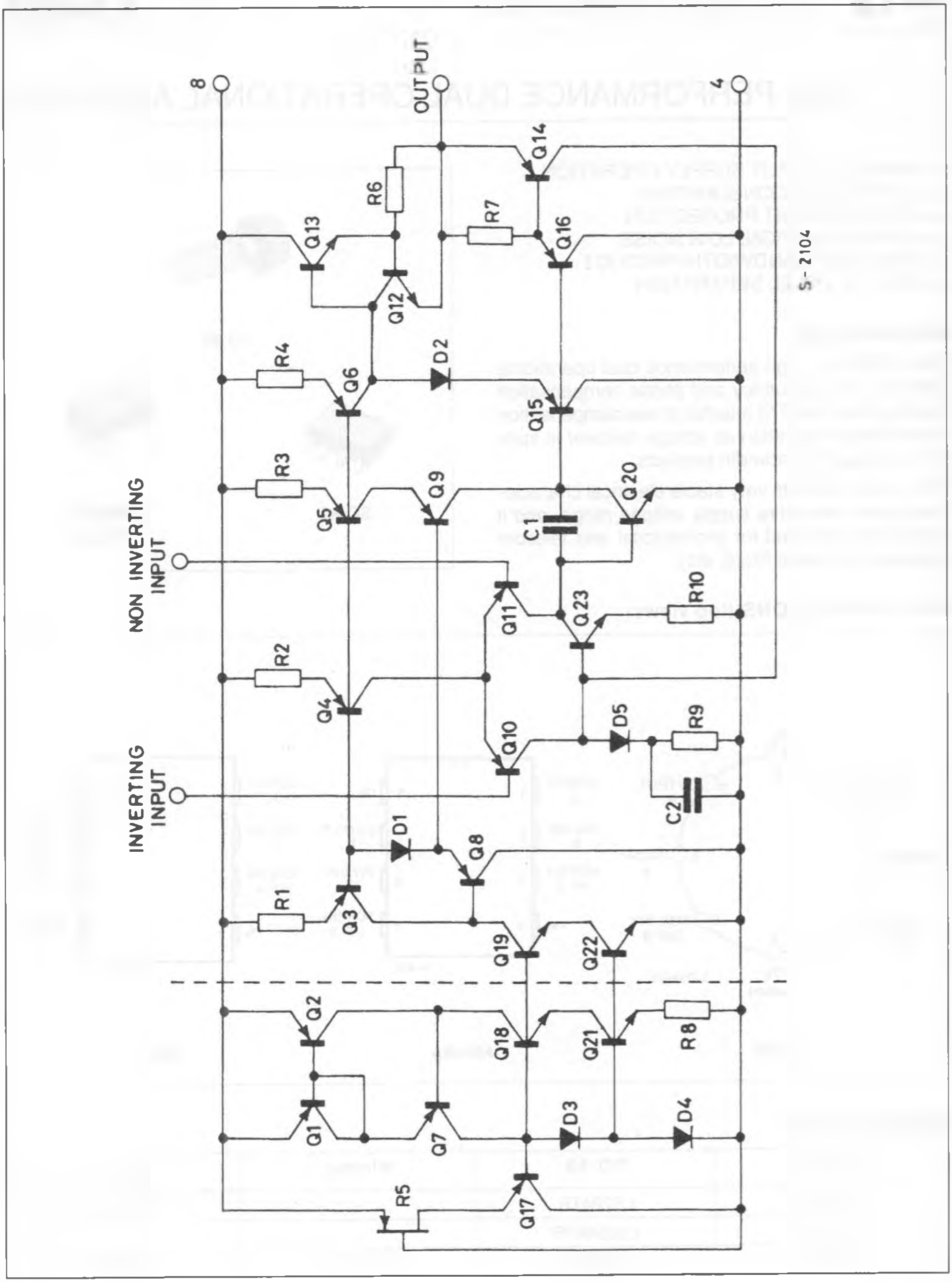


TO-99 | Minidip | SO-8

ORDER CODES

Type	TO-99	Minidip	SO-8
LS204	LS204TB	–	LS204M
LS204A	LS204ATB	–	–
LS204C	LS204CTB	LS204CB	LS204CM

SCHEMATIC DIAGRAM



SGS-THOMSON MICROELECTRONICS

ABSOLUTE MAXIMUM RATINGS

Symbol	Parameter		TO-99	Minidip	uPackage
V_s	Supply Voltage		± 18V		
V_i	Input Voltage		$\pm V_s$		
V_i	Differential Input Voltage		$\pm (V_s - 1)$		
T_{op}	Operating Temperature for	**LS204** **LS204A** **LS204C**	– 25 to 85°C – 55 to 125°C 0 to 70°C		
P_{tot}	Power Dissipation at T_{amb} = 70°C		520mW	665mW	400mW
T_j	Junction Temperature		150°C	150°C	150°C
T_{stg}	Storage Temperature		– 65 to 150°C	– 55 to 150°C	– 55 to 150°C

THERMAL DATA

			TO-99	Minidip	SO-8J
$R_{thj\text{-}amb}$	Thermal Resistance Junction-ambient	Max	155°C/W	120°C/W	200°C/W

ELECTRICAL CHARACTERISTICS (V_s = ± 15V, T_{amb} = 25°C, unless otherwise specified)

Symbol	Parameter	Test Conditions	LS204/LS204A			LS204C			Unit
			Min.	Typ.	Max.	Min.	Typ.	Max.	
I_s	Supply Current			0.7	1.2		0.8	1.5	mA
I_b	Input Bias Current			50	150		100	300	nA
		$T_{min} < T_{op} < T_{max}$			300			700	nA
R_i	Input Resistance	f = 1KHz		1			0.5		MΩ
V_{os}	Input Offset Voltage	$R_g \le 10K\Omega$		0.5	2.5		0.5	3.5	mV
		$R_g \le 10K\Omega$ $T_{min} < T_{op} < T_{max}$			3.5			5	mV
$\frac{\Delta V_{os}}{\Delta T}$	Input Offset Voltage Drift	$R_g = 10K\Omega$ $T_{min} < T_{op} < T_{max}$		5			5		µV/°C
I_{os}	Input Offset Current			5	20		12	50	nA
		$T_{min} < T_{op} < T_{max}$			40			100	nA
$\frac{\Delta I_{os}}{\Delta T}$	Input Offset Current Drift	$T_{min} < T_{op} < T_{max}$		0.08			0.1		$\frac{nA}{°C}$
I_{sc}	Output Short Circuit Current			23			23		mA
G_v	Large Signal Open Loop Voltage Gain	$T_{min} < T_{op} < T_{max}$ $R_L = 2K\Omega$ $V_s = \pm 15V$ $V_s = \pm 4V$	90	100 95		86	100 95		dB
B	Gain-bandwidth Product	f = 20KHz	1.8	3		1.5	2.5		MHz
e_N	Total Input Noise Voltage	f = 1KHz $R_g = 50\Omega$ $R_g = 1K\Omega$ $R_g = 10K\Omega$		8 10 18	15		10 12 20		$\frac{nV}{\sqrt{Hz}}$

ELECTRICAL CHARACTERISTICS (continued)

Symbol	Parameter	Test Conditions	LS204/LS204A			LS204C			Unit
			Min.	Typ.	Max.	Min.	Typ.	Max.	
d	Distortion	G_v = 20dB R_L = 2KΩ V_o = 2 V_{PP} f = 1KHZ		0.03	0.1		0.03	0.1	%
V_o	DC Output Voltage Swing	R_L = 2KΩ V_s = ± 15V V_s = ± 4 V	± 13	± 3		± 13	± 3		V
V_o	Large Signal Voltage Swing	R_L = 10KΩ f = 10KHz		28			28		V_{pp}
SR	Slew Rate	Unity Gain R_L = 2KΩ	0.8	1.5			1		V/μs
CMR	Common Mode Rejection	V_i = 10V $T_{min} < T_{op} < T_{max}$	90			86			dB
SVR	Supply Voltage Rejection	V_i = 1V f = 100Hz $T_{min} < T_{op} < T_{max}$	90			86			dB
CS	Channel Separation	f = 1KHz 100	120			120			dB

Note :

Temp.	LS204	LS204A	LS204C
$T_{min.}$	– 25°C	– 55°C	0°C
$T_{max.}$	+ 85°C	+ 125°C	+ 70°C

Figure 1: Supply Current vs. Supply Voltage.

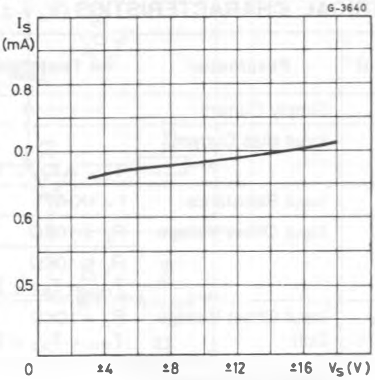


Figure 2 : Supply Current vs. Ambient Temperature.

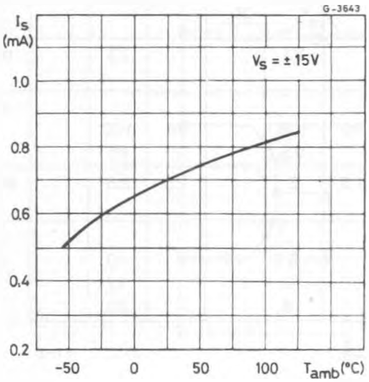


Figure 3 : Output Short Circuit Current vs. Ambient Temperature.

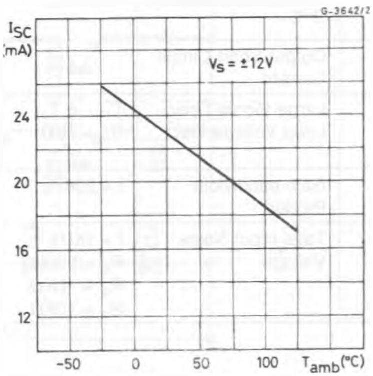


Figure 4: Open Loop Frequency and Phase Response.

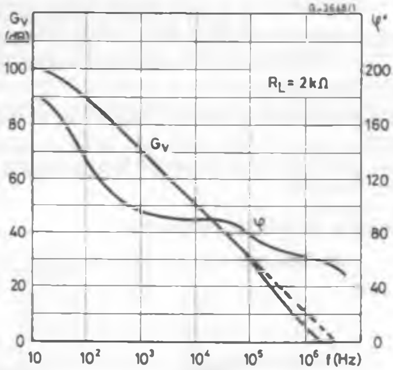


Figure 5: Open Loop Gain vs. Ambient Temperature.

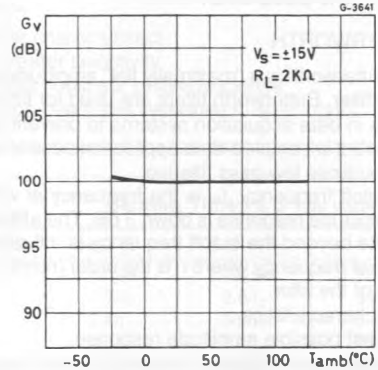


Figure 6 : Supply Voltage Rejection vs. Frequency.

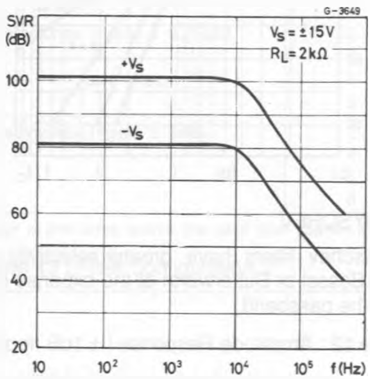


Figure 7 : Large Signal Frequency Response.

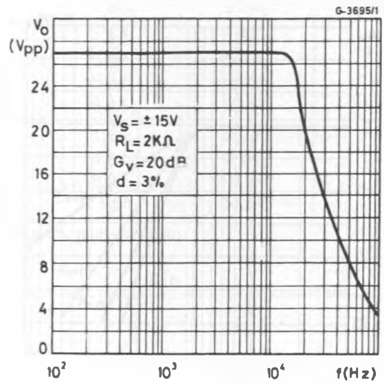


Figure 8 : Output Voltage Swing vs. Load Resistance.

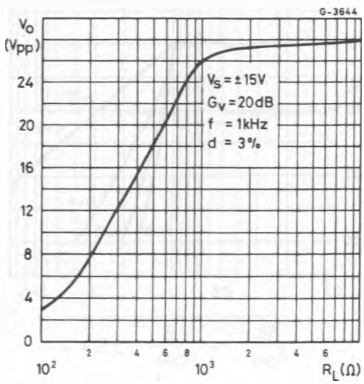
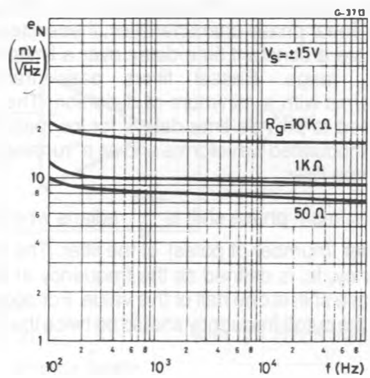


Figure 9 : Total Input Noise vs. Frequency.



APPLICATION INFORMATION

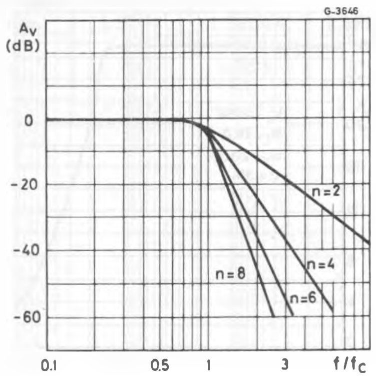
Active low-pass filter :

BUTTERWORTH

The Butterworth is a "maximally flat" amplitude response filter. Butterworth filters are used for filtering signals in data acquisition systems to prevent aliasing errors in sampled-data applications and for general purpose low-pass filtering.
The cutoff frequency, f_c, is the frequency at which the amplitude response is down 3 dB. The attenuation rate beyond the cutoff frequency is n6 dB per octave of frequency where n is the order (number of poles) of the filter.
Other characteristics :

- Flattest possible amplitude response.
- Excellent gain accuracy at low frequency end of passband.

Figure 10 : Amplitude Response.



BESSEL

The Bessel is a type of "linear phase" filter. Because of their linear phase characteristics, these filters approximate a constant time delay over a limited frequency range. Bessel filters pass transient waveforms with a minimum of distortion. They are also used to provide time delays for low pass filtering of modulated waveforms and as a "running average" type filter.

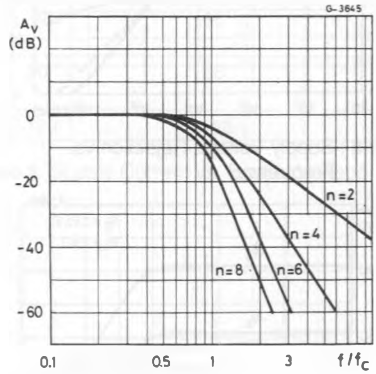
The maximum phase shift is $\frac{-n\pi}{2}$ radians where n is the order (number of poles) of the filter. The cutoff frequency, fc, is defined as the frequency at which the phase shift is one half of this value. For accurate delay, the cutoff frequency should be twice the maximum signal frequency. The following table can be used to obtain the – 3dB frequency of the filter

	2 pole	4 Pole	6 Pole	8 Pole
– 3dB Frequency	0.77 f_c	0.67 f_c	0.57 f_c	0.50 f_c

Other characteristics :

- Selectivity not as great as Chebyschev or Butterworth.
- Very little overshoot response to step inputs.
- Fast rise time.

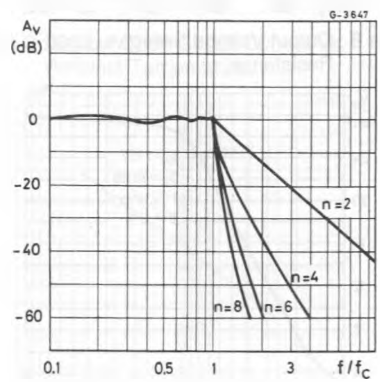
Figure 11 : Amplitude Response.



CHEBYSCHEV

Chebyschev filters have greater selectivity than either Bessel or Butterworth at the expense of ripple in the passband.

Figure 12 : Amplitude Response (± 1dB ripple).



APPLICATION INFORMATION (continued)

Chebyschev filters are normally designed with peak-to-peak ripple values from 0.2 dB to 2 dB.

Increased ripple in the passband allows increased attenuation above the cutoff frequency.
The cutoff frequency is defined as the frequency at which the amplitude response passes through the specified maximum ripple band and enters the stop band.

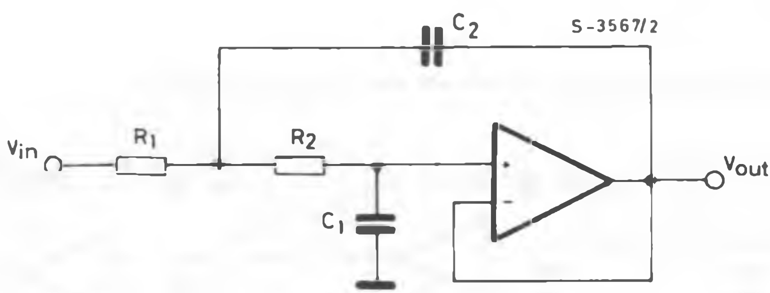
Other characteristics :
- Greater selectivity
- Very nonlinear phase response
- High overshoot response to step inputs

The table below shows the typical overshoot and settling time response of the low pass filters to a step input.

	Number of Poles	Peak Overshoot	Settling Time (% of final value)		
		% Overshoot	± 1%	± 0 .1%	± 0.01%
Butterworth	2	4	$1.1/f_c$sec.	$1.7/f_c$sec.	$1.9/f_c$sec.
	4	11	$1.7/f_c$	$2.8/f_c$	$3.8/f_c$
	6	14	$2.4/f_c$	$3.9/f_c$	$5.0/f_c$
	8	16	$3.1/f_c$	$5.1/f_c$	$7.1/f_c$
Bessel	2	0.4	$0.8/f_c$	$1.4/f_c$	$1.7/f_c$
	4	0.8	$1.0/f_c$	$1.8/f_c$	$2.4/f_c$
	6	0.6	$1.3/f_c$	$2.1/f_c$	$2.7/f_c$
	8	0.3	$1.6/f_c$	$2.3/f_c$	$3.2/f_c$
Chebyschev (ripple ± 0.25dB)	2	11	$1.1/f_c$	$1.6/f_c$	–
	4	18	$3.0/f_c$	$5.4/f_c$	–
	6	21	$5.9/f_c$	$10.4/f_c$	–
	8	23	$8.4/f_c$	$16.4/f_c$	–
Chebyschev (ripple ± 1dB)	2	21	$1.6/f_c$	$2.7/f_c$	–
	4	28	$4.8/f_c$	$8.4/f_c$	–
	6	32	$8.2/f_c$	$16.3/f_c$	–
	8	34	$11.6/f_c$	$24.8/f_c$	–

Design of 2nd order active low pass filter (Sallen and Key configuration unity gain-op-amp).

Figure 13 : Filter Configuration.



$$\frac{V_o}{V_i} = \frac{1}{1 + 2\xi \frac{S}{\omega c} + \frac{S^2}{\omega c^2}}$$

Where :

$\omega_c = 2\pi f_c$ with f_c = cutoff frequency

ξ = damping factor.

APPLICATION INFORMATION (continued)

Three parameters are needed to characterise the frequency and phase response of a 2nd order active filter : the gain (G_V), the damping factor (ξ) or the Q-factor ($Q = (2\,\xi)^{-1}$), and the cutoff frequency (f_c).

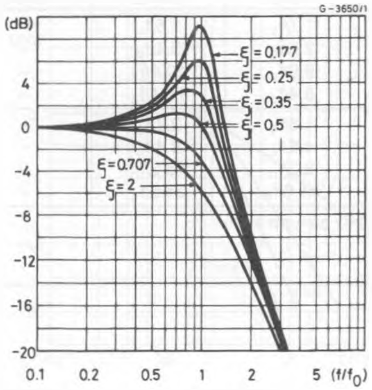
The higher order responses are obtained wit a series of 2nd order sections. A simple RC section is introduced when an odd filter is required.

The choice of 'ξ' (or Q-factor) determines the filter response (see table).

Table 1.

Filter Response	ξ	Q	Cutoff Frequency f_c
Bessel	$\frac{\sqrt{3}}{2}$	$\frac{1}{\sqrt{3}}$	Frequency at which Phase Shift is – 90°C
Butterworth	$\frac{\sqrt{2}}{2}$	$\frac{1}{\sqrt{2}}$	Frequency at Which G_v = – 3dB
Chebyschev	$< \frac{\sqrt{2}}{2}$	$> \frac{1}{\sqrt{2}}$	Frequency at which the amplitude response passes through specified max. ripple band and enters the stop band.

Figure 14 : Filter Response vs. Damping Factor.



Fixed R = R1 = R2, we have (see fig. 13)

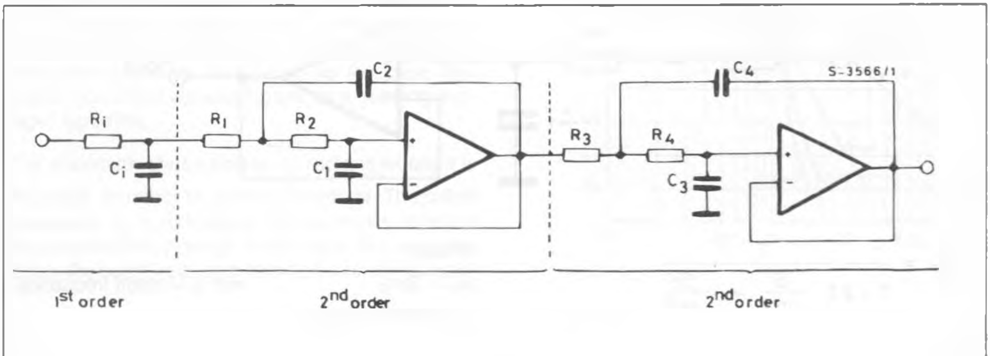
$$C_1 = \frac{1}{R} \quad \frac{\xi}{\omega_c}$$

$$C_2 = \frac{1}{R} \quad \frac{1}{\xi\omega_c}$$

The diagram of fig.14 shows the amplitude response for different values of damping factor ξ in

EXAMPLE

Figure 15 : 5th Order Low Pass Filter (Butterworth) with Unity Gain Configuration.



SGS-THOMSON MICROELECTRONICS

APPLICATION INFORMATION (continued)

In the circuit of fig. 15, for f_c = 3.4 KHz and $R_i = R_1 = R_2 = R_3 = R_4$ =10 KΩ, we obtain :

$$C_i = 1.354 \cdot \frac{1}{R} \cdot \frac{1}{2\pi f_c} = 6.33nF$$

$$C_1 = 0.421 \cdot \frac{1}{R} \cdot \frac{1}{2\pi f_c} = 1.97nF$$

$$C_2 = 1.753 \cdot \frac{1}{R} \cdot \frac{1}{2\pi f_c} = 8.20nF$$

$$C_3 = 0.309 \cdot \frac{1}{R} \cdot \frac{1}{2\pi f_c} = 1.45nF$$

$$C_4 = 3.325 \cdot \frac{1}{R} \cdot \frac{1}{2\pi f_c} = 15.14nF$$

The attenuation of the filter is 30 dB at 6.8 KHz and better than 60 dB at 15 KHz.

The same method, referring to Tab. II and fig. 16, is used to design high-pass filter. In this case the damping factor is found by taking the reciprocal of the numbers in Tab. II. For f_c = 5 KHz and $C_i = C_1 = C_2 = C_3 = C_4$ = 1 nF we obtain :

$$R_i = \frac{1}{1.354} \cdot \frac{1}{C} \cdot \frac{1}{2\pi f_c} = 23.5K\Omega$$

$$R_1 = \frac{1}{0.421} \cdot \frac{1}{C} \cdot \frac{1}{2\pi f_c} = 75.6K\Omega$$

$$R_2 = \frac{1}{1.753} \cdot \frac{1}{C} \cdot \frac{1}{2\pi f_c} = 18.2K\Omega$$

$$R_3 = \frac{1}{0.309} \cdot \frac{1}{C} \cdot \frac{1}{2\pi f_c} = 103K\Omega$$

$$R_4 = \frac{1}{3.325} \cdot \frac{1}{C} \cdot \frac{1}{2\pi f_c} = 9.6K\Omega$$

Table 2 : Damping Factor for Low-pass Butterworth Filters.

Order	C_i	C_1	C_2	C_3	C_4	C_5	C_6	C_7	C_8
2		0.707	1.41						
3	1.392	0.202	3.54						
4		0.92	1.08	0.38	2.61				
5	1.354	0.421	1.75	0.309	3.235				
6		0.966	1.035	0.707	1.414	0.259	3.86		
7	1.336	0.488	1.53	0.623	1.604	0.222	4.49		
8		0.98	1.02	0.83	1.20	0.556	1.80	0.195	5.125

Figure 16 : 5_{th} Order High-pass Filter (Butterworth) with Unity Gain Configuration.